

Forensic analysis of the TESLA-pickup signal-processing unit



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DESY-TEMF Meeting
June 28, 2024
TEMF, Darmstadt

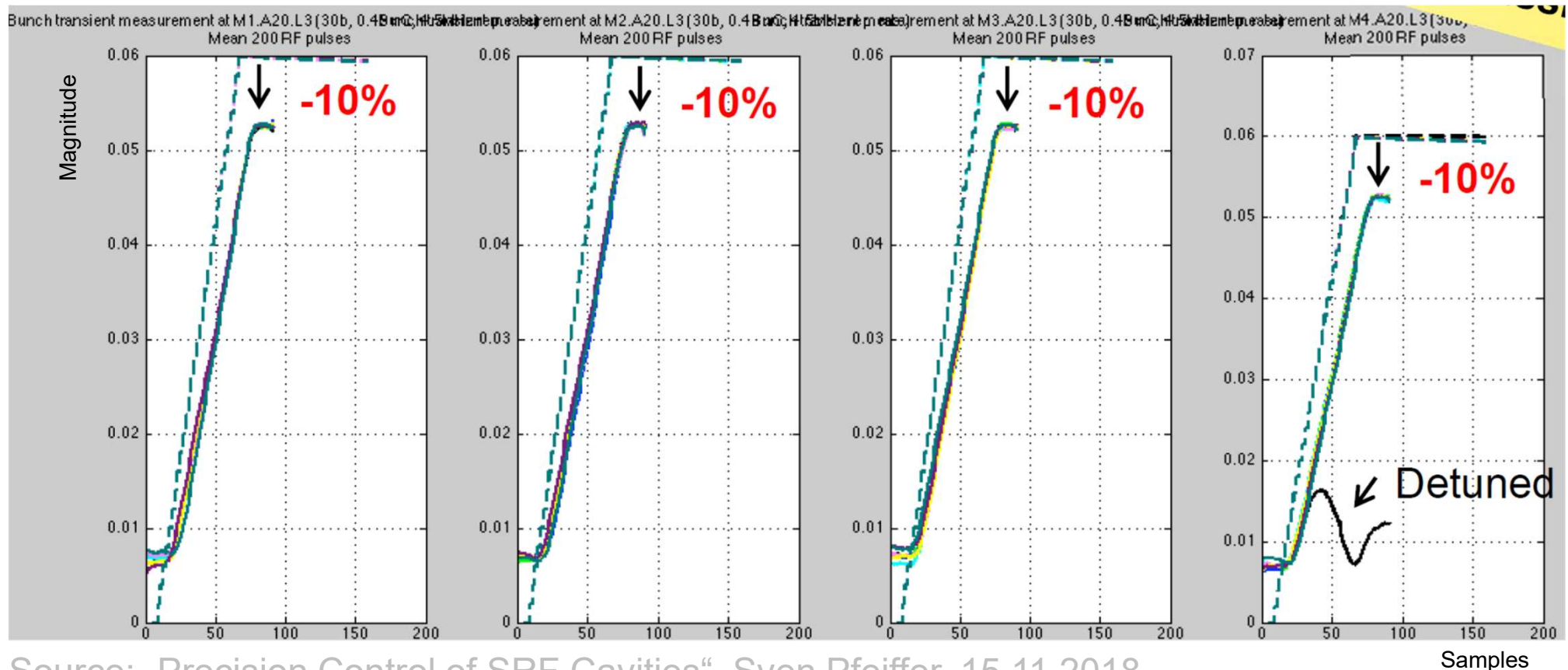


- Motivation
- Computational Modeling
 - Excitation of a 9-Cell TESLA Cavity
 - Klystron (Steady State Case, Single-Mode Operation)
 - Moving Particles (Transient Behavior, Multi-Mode Operation)
 - Measurement of the Field Magnitude in the Cavity
 - Trace the Signal from the Pickup Antenna to the Digital Fourier Analysis
 - Apply the Numerical Model to Representative Signal Patterns
- Summary / Outlook

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Motivation

- Beam Loading of a 9 Cell TESLA 1.3 GHz Cavity
 - Comparison of theory with measurement



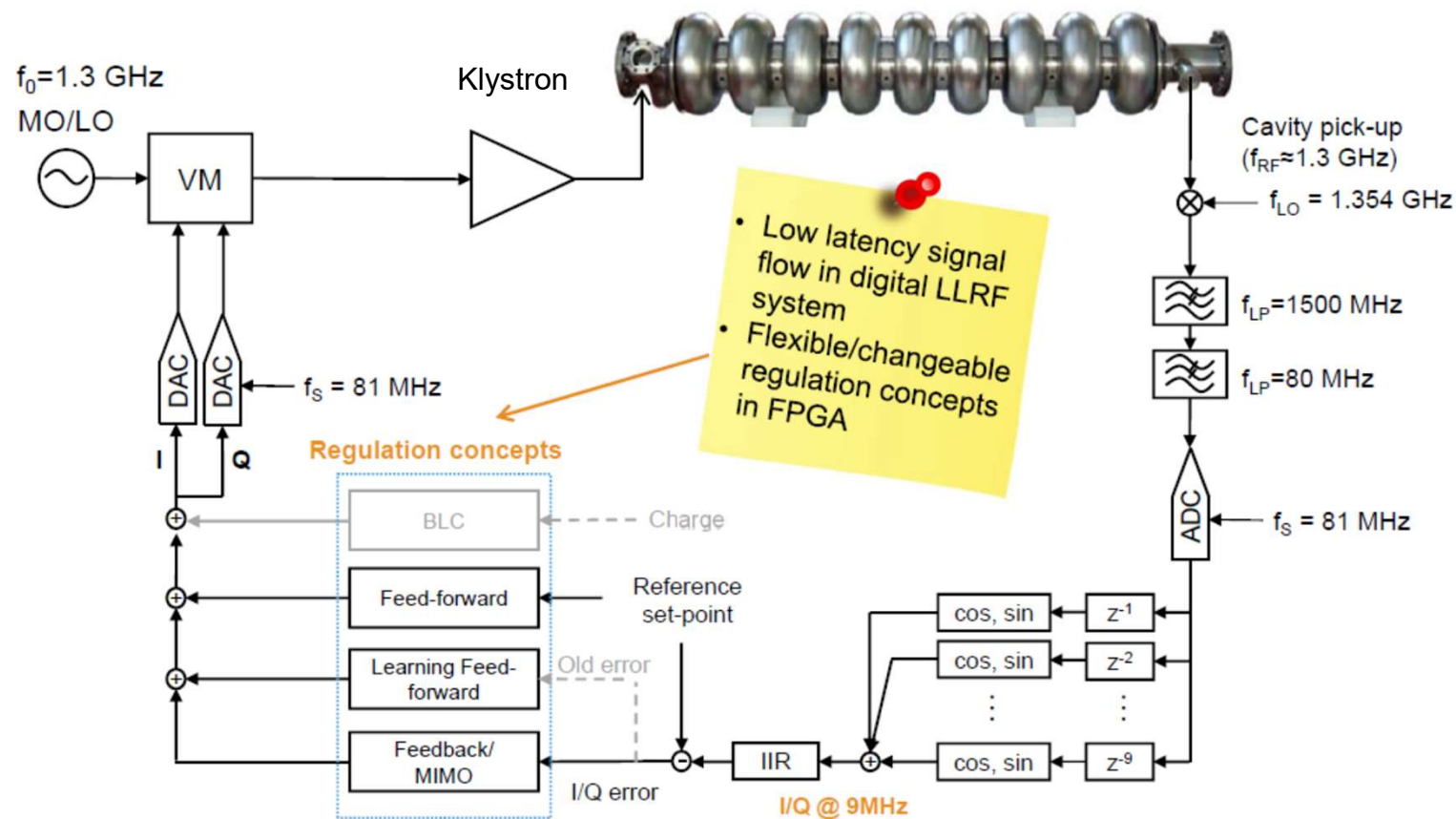
Source: „Precision Control of SRF Cavities“, Sven Pfeiffer, 15.11.2018

Motivation



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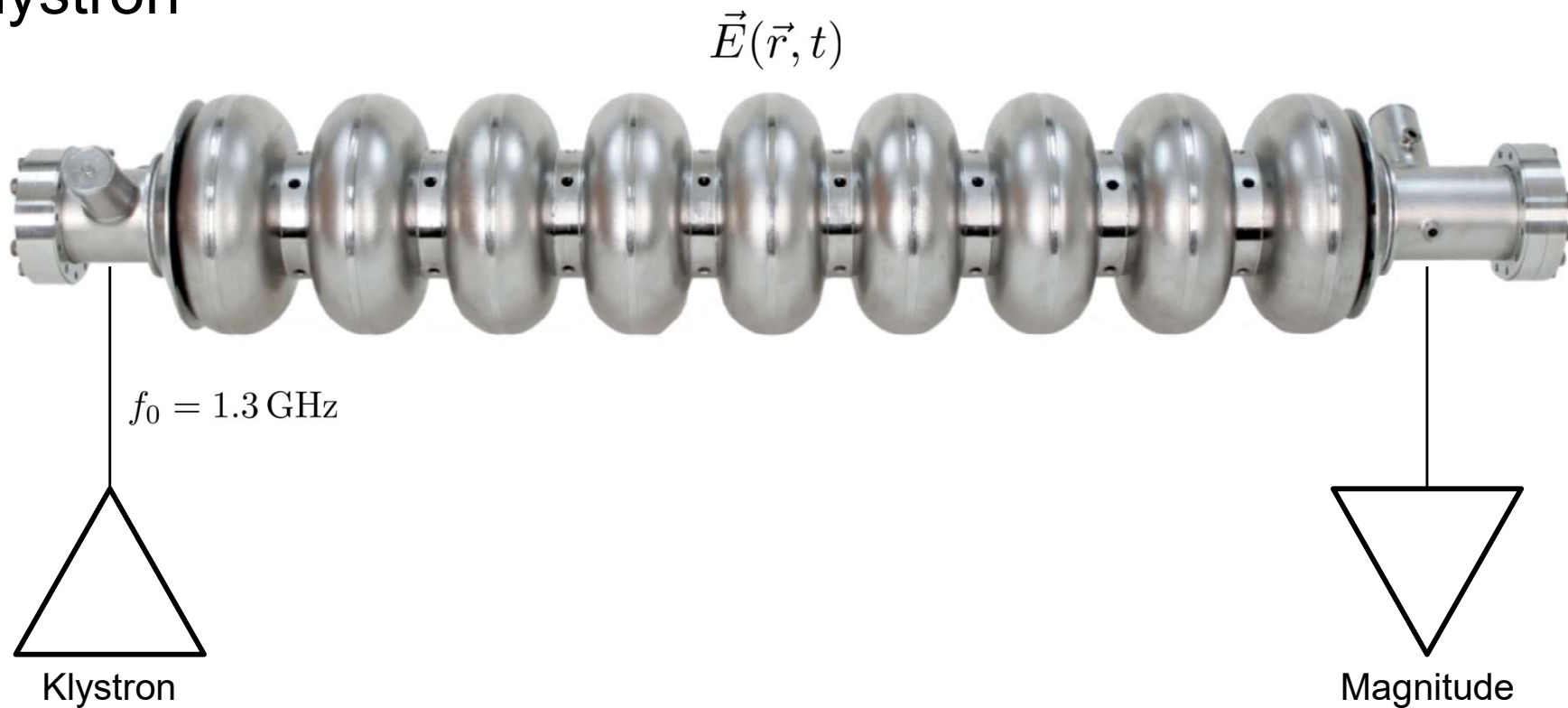
■ SRF Cavity Regulation



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- Cavity Excitation
 - Klystron



Relation between measured
magnitude of the pickup signal and
the field strength in the cavity?

Numerical Modeling



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- Cavity Modeling

- Photograph



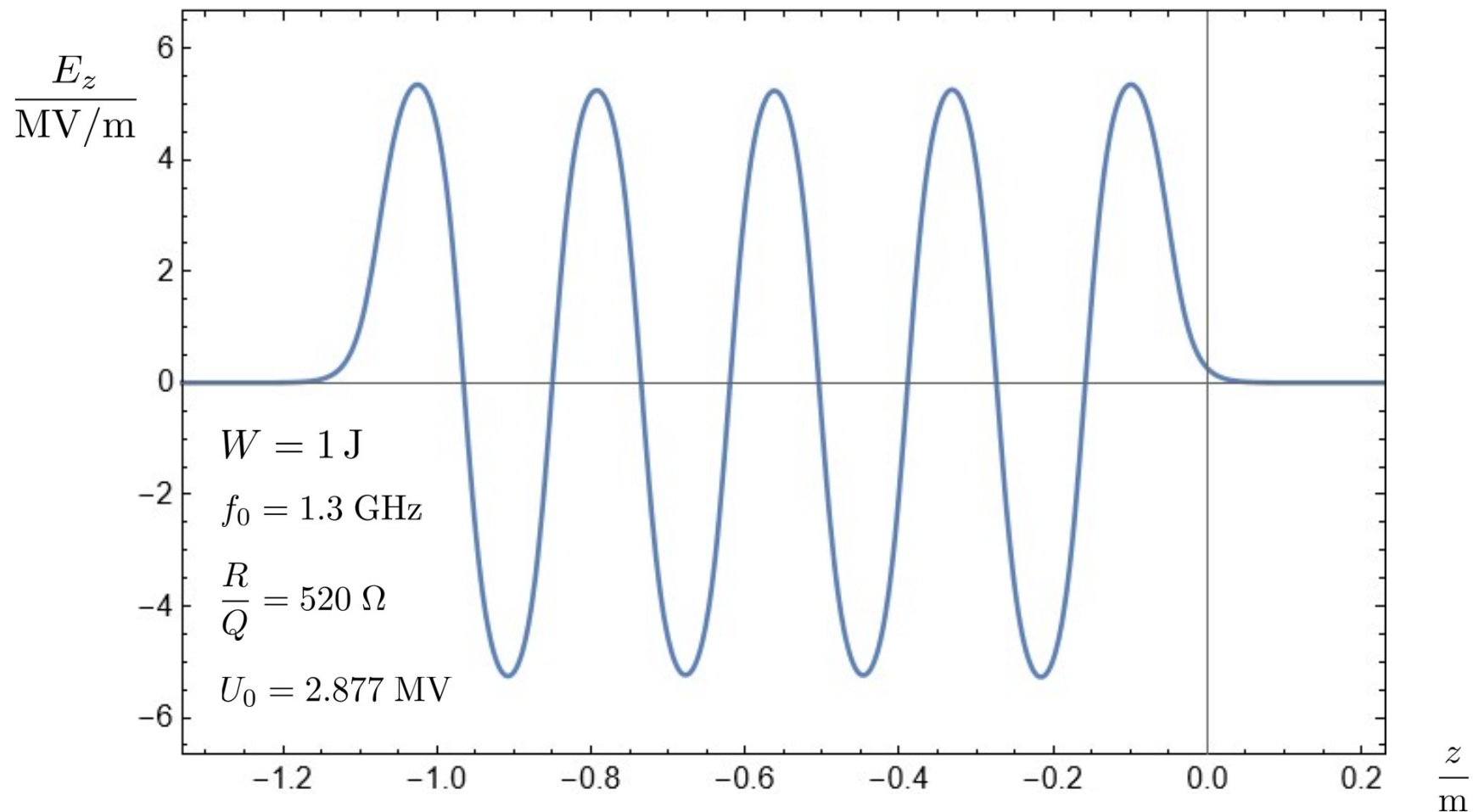
<http://newsline.linearcollider.org>

- Numerical model



CST Studio Suite 2024

- Cavity Field Distribution for the Accelerating Mode



Numerical Modeling



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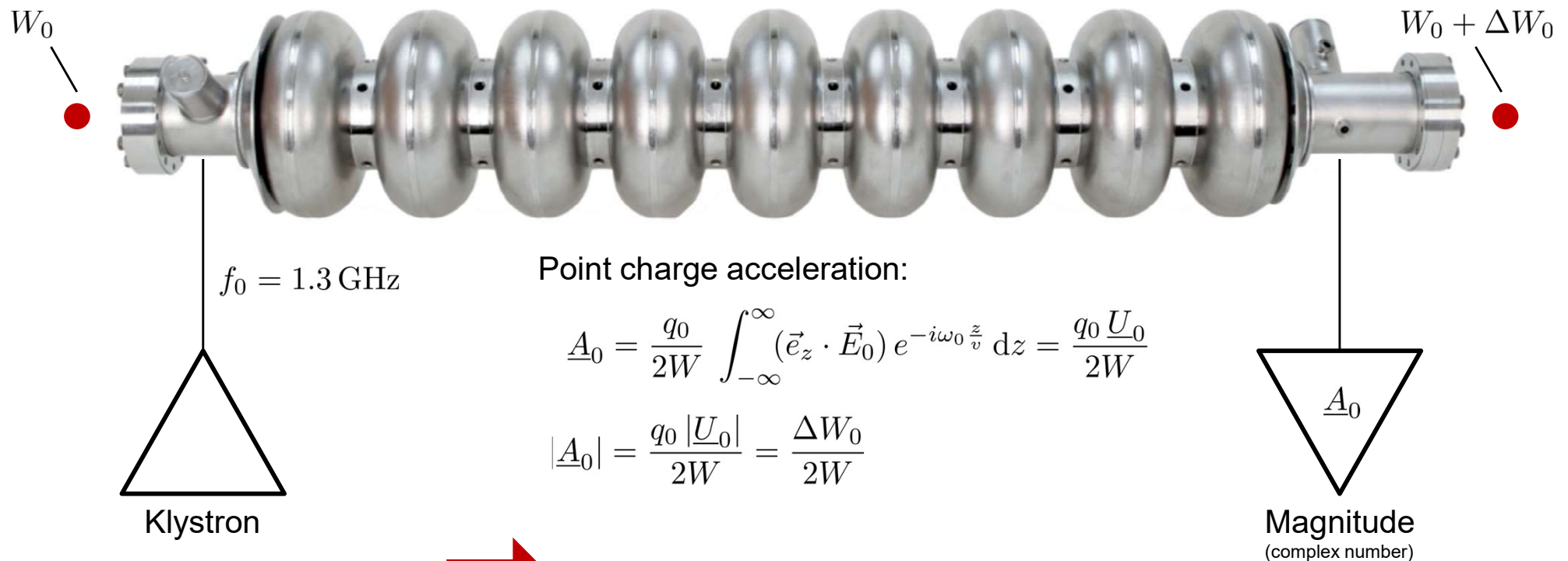
■ Cavity Excitation - Klystron

$$\iiint_V \varepsilon \vec{E}_\nu \cdot \vec{E}_\eta dV = \delta_{\nu,\eta} 2W$$

$$W \stackrel{!}{=} 1 \text{ J}$$

$$\vec{E}(\vec{r}, t) = a_0(t) \vec{E}_0(\vec{r})$$

$$a_0(t) = \Re(\underline{A}_0 e^{i\omega_0 t})$$



Scaling is independent of the charge.

Numerical Modeling



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■ Cavity Excitation - Moving Particle

$$\iiint_V \varepsilon \vec{E}_\nu \cdot \vec{E}_\eta dV = \delta_{\nu,\eta} 2W$$

$$W \stackrel{!}{=} 1 \text{ J}$$

$$\Delta W = \sum_{\nu=1}^{\infty} \Delta W_\nu$$

$$\vec{E}(\vec{r}, t) = \vec{E}_P(\vec{r}, t) + \sum_{\nu=1}^{\infty} a_\nu(t) \vec{E}_\nu(\vec{r})$$

$$a_\nu(t) = \Re(\underline{A}_\nu e^{i\omega_\nu t})$$



Point charge excitation:

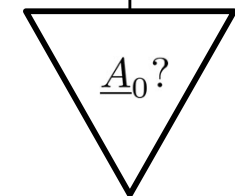
$$\underline{A}_\nu = \frac{q_0}{2W} \int_{-\infty}^{\infty} (\vec{e}_z \cdot \vec{E}_\nu) e^{-i\omega_\nu \frac{z}{v}} dz = \frac{q_0 \underline{U}_\nu}{2W}$$

$$|\underline{A}_\nu| = \frac{q_0 |\underline{U}_\nu|}{2W} = \frac{\Delta W_\nu}{2W} = q_0 \sqrt{\left(\frac{R}{Q}\right)_\nu \frac{\omega_\nu}{2W}}$$

$$\Delta W = q_0 |\underline{U}_0|$$

$$Q = \frac{\omega W}{P}$$

$$R = \frac{|\underline{U}_0|^2}{2P}$$



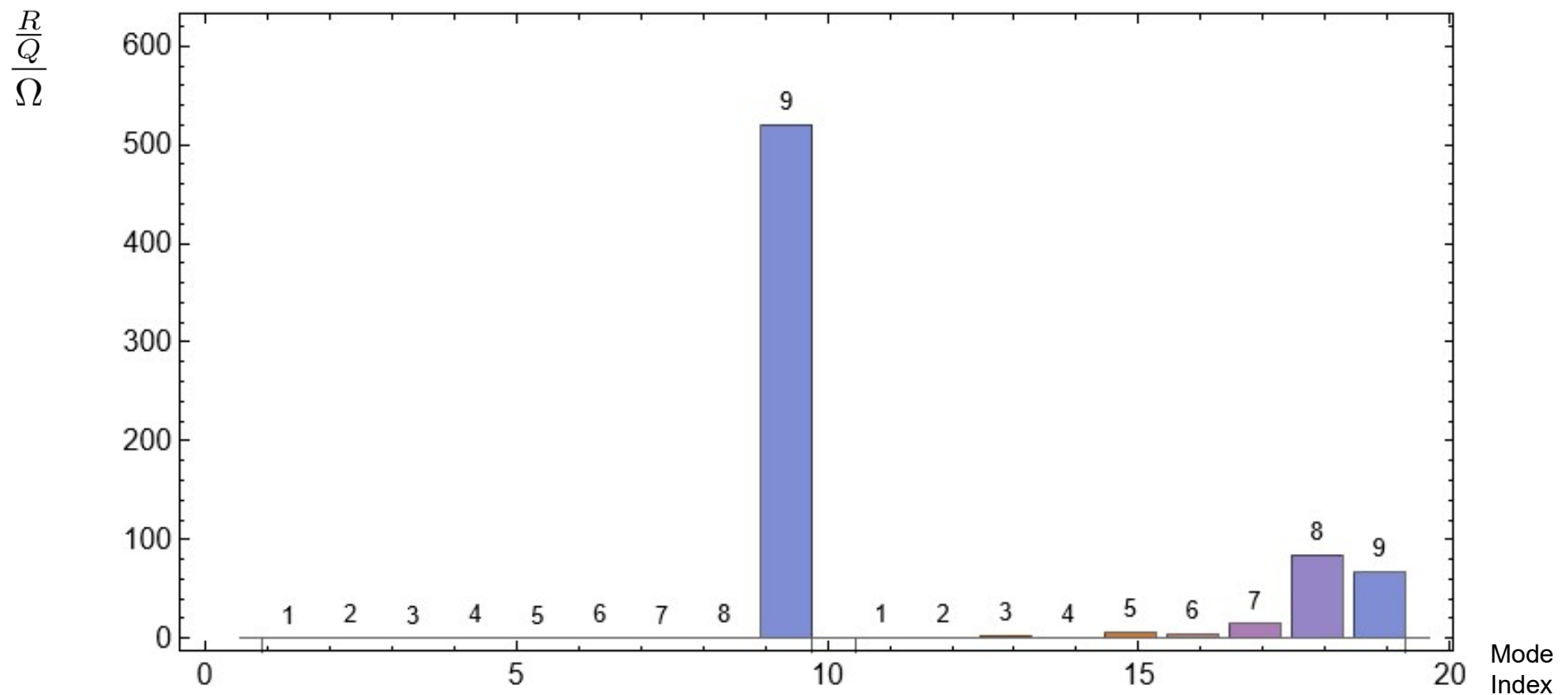
Magnitude
(complex number)

Numerical Results



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- Data from Mode Atlas
 - First and Second Monopole Passband

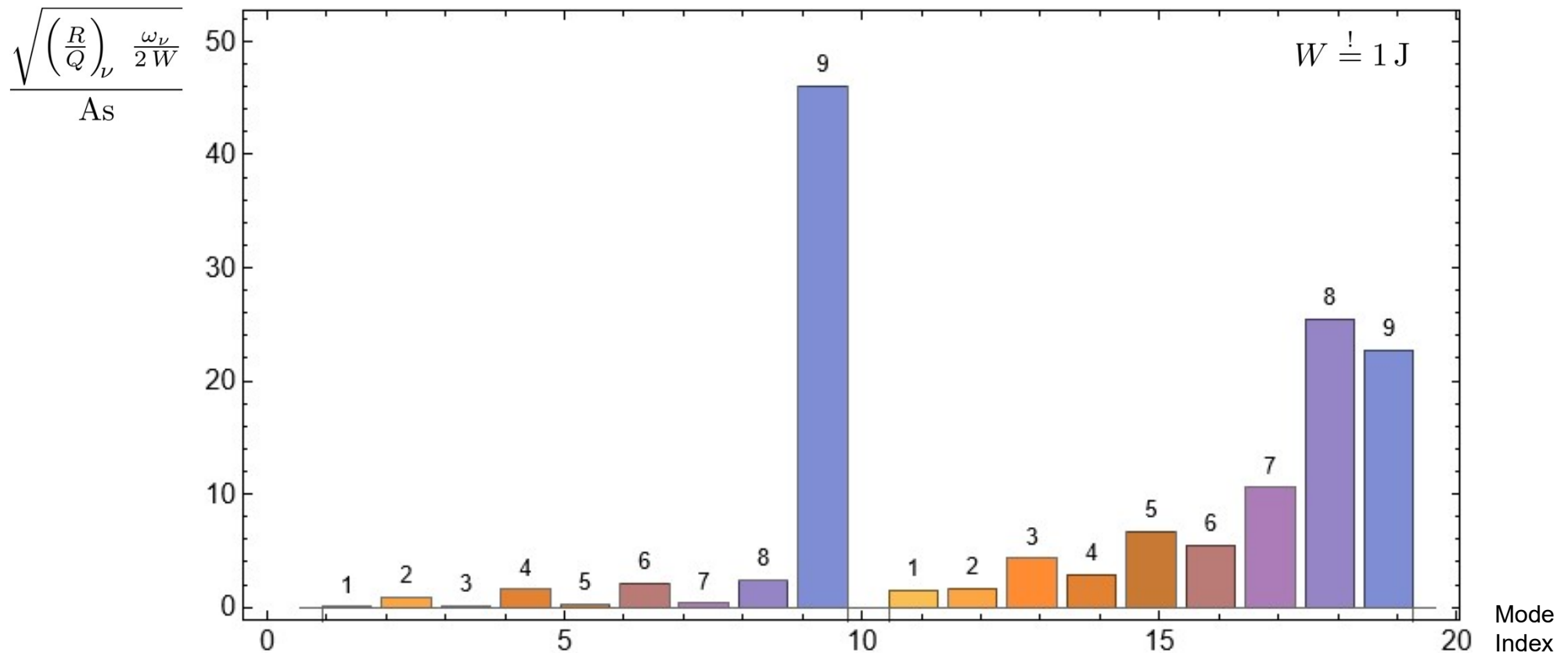


Numerical Results



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- Mode Atlas
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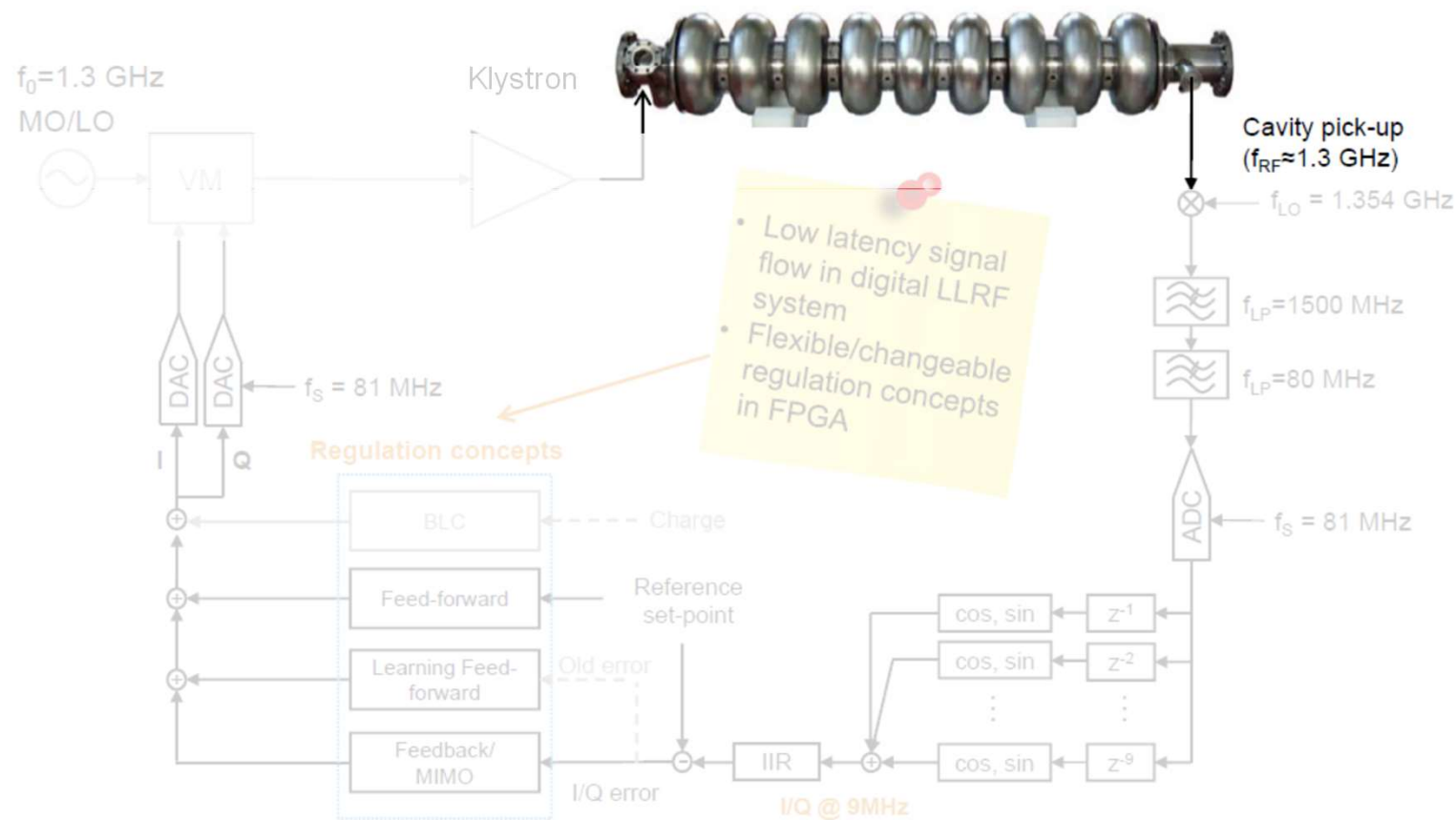


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Numerical Results



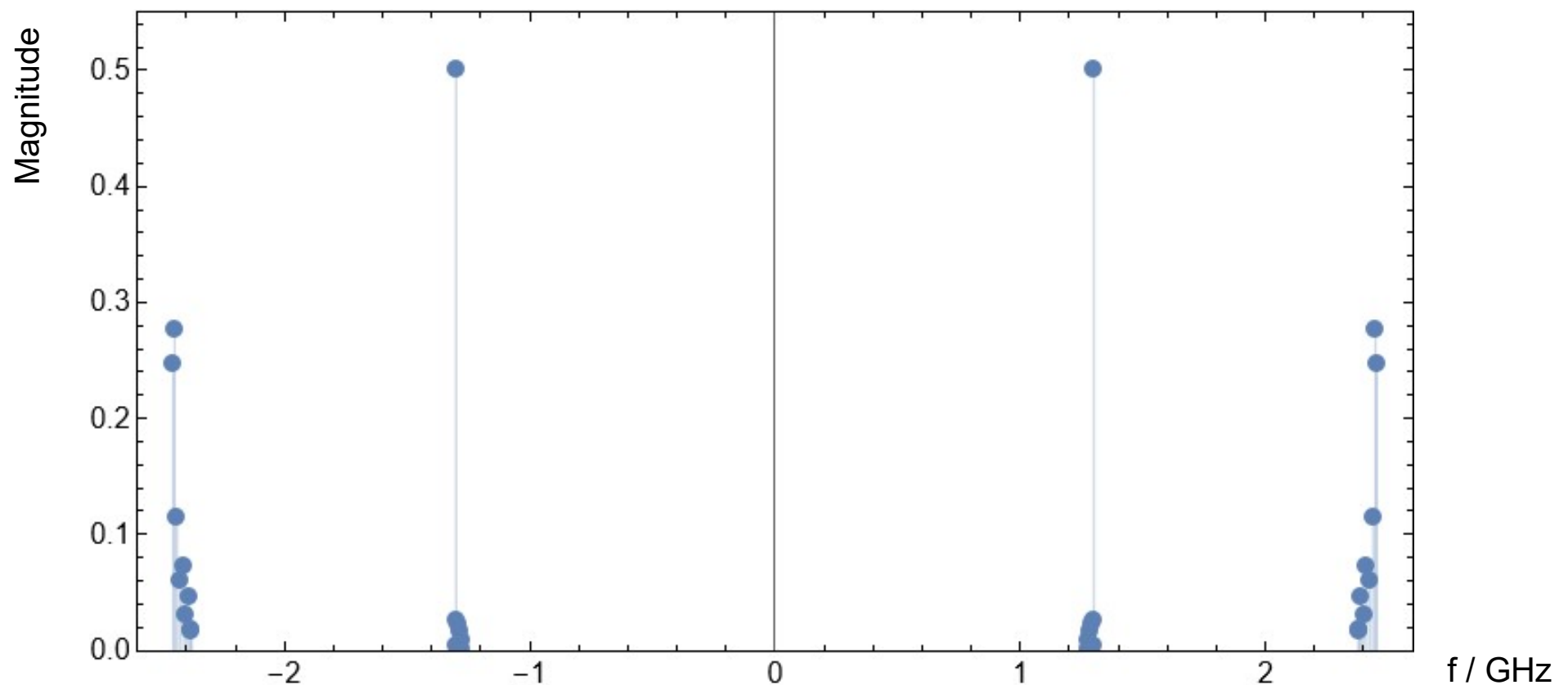
▪ SRF Cavity Regulation



Source: „Precision Control of SRF Cavities“, Sven Pfeiffer, 15.11.2018

Numerical Results

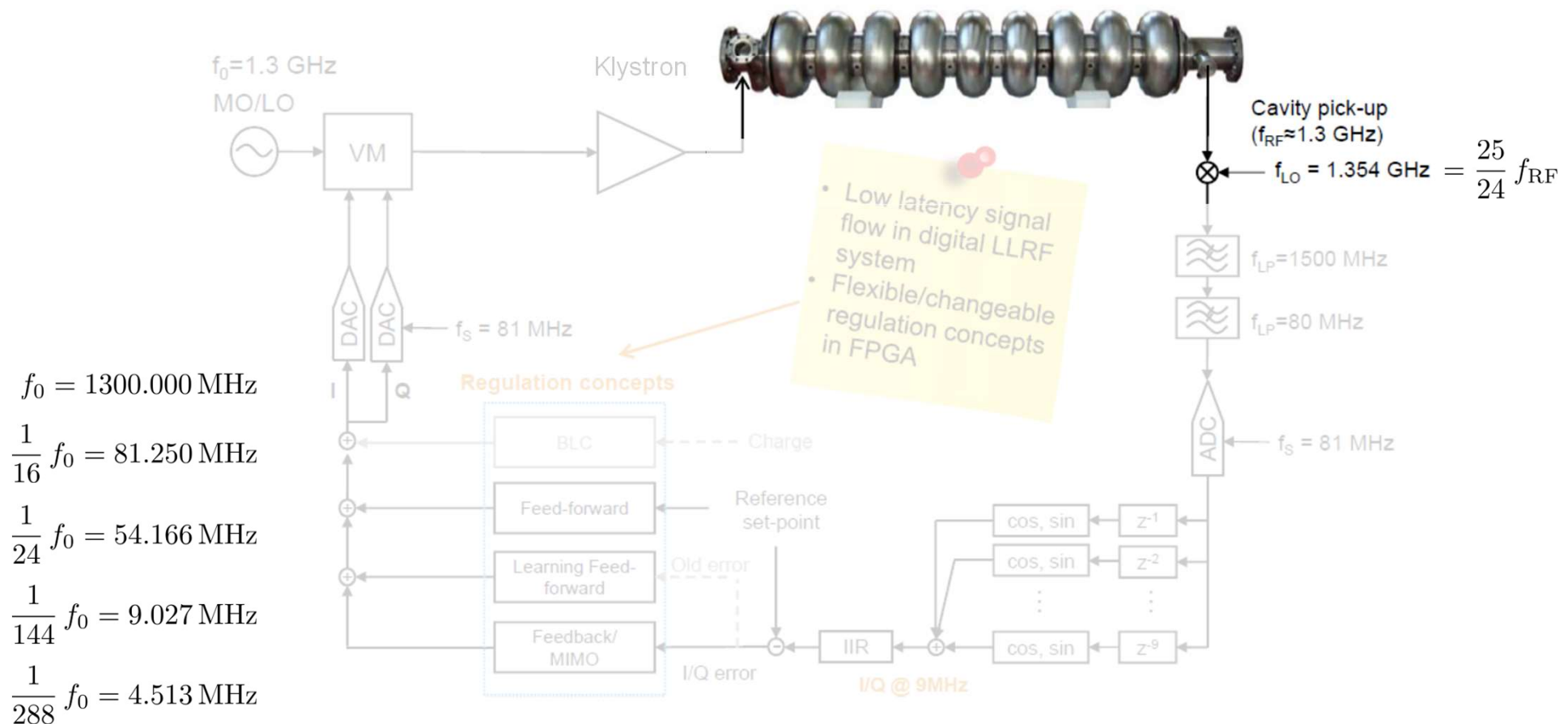
- Spectrum after Point-Charge Excitation
 - First and Second Monopole Passband



Numerical Results



▪ SRF Cavity Regulation

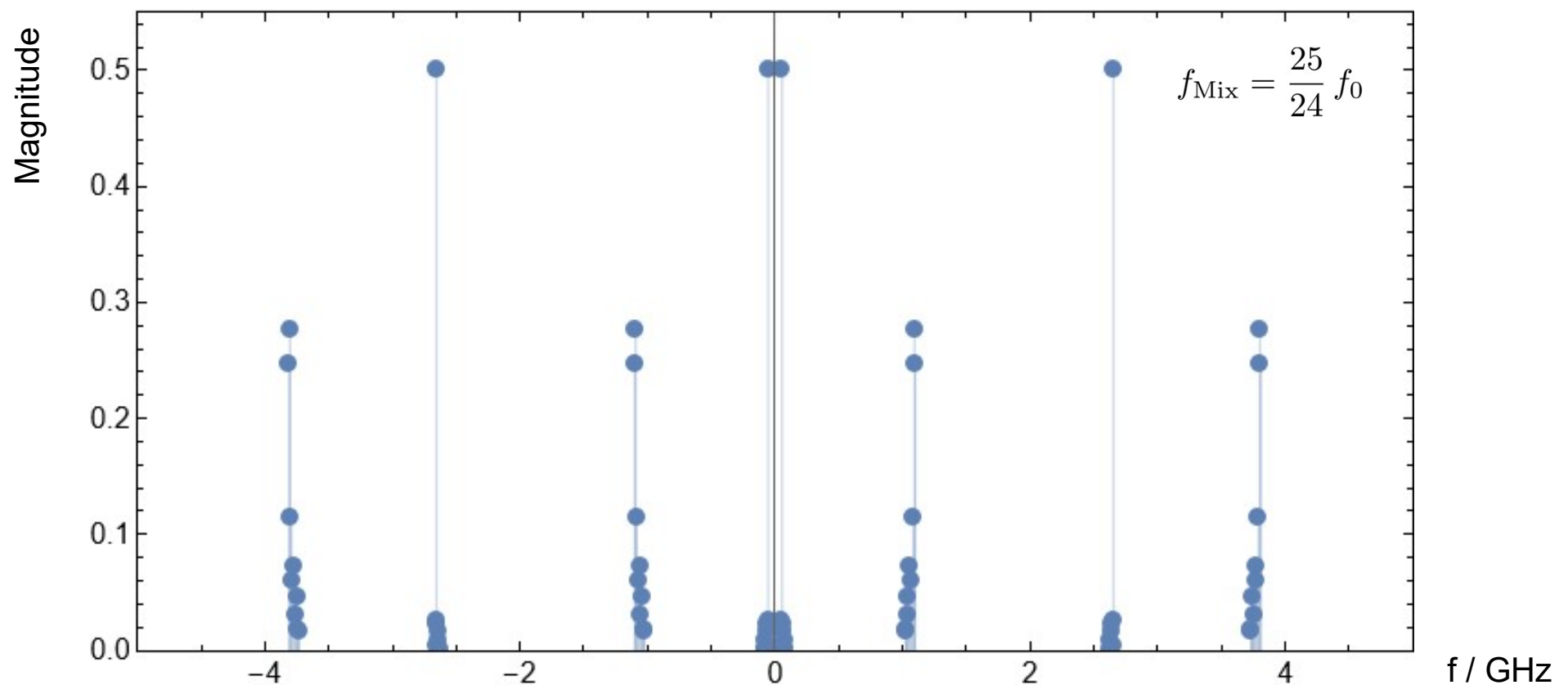


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Numerical Results

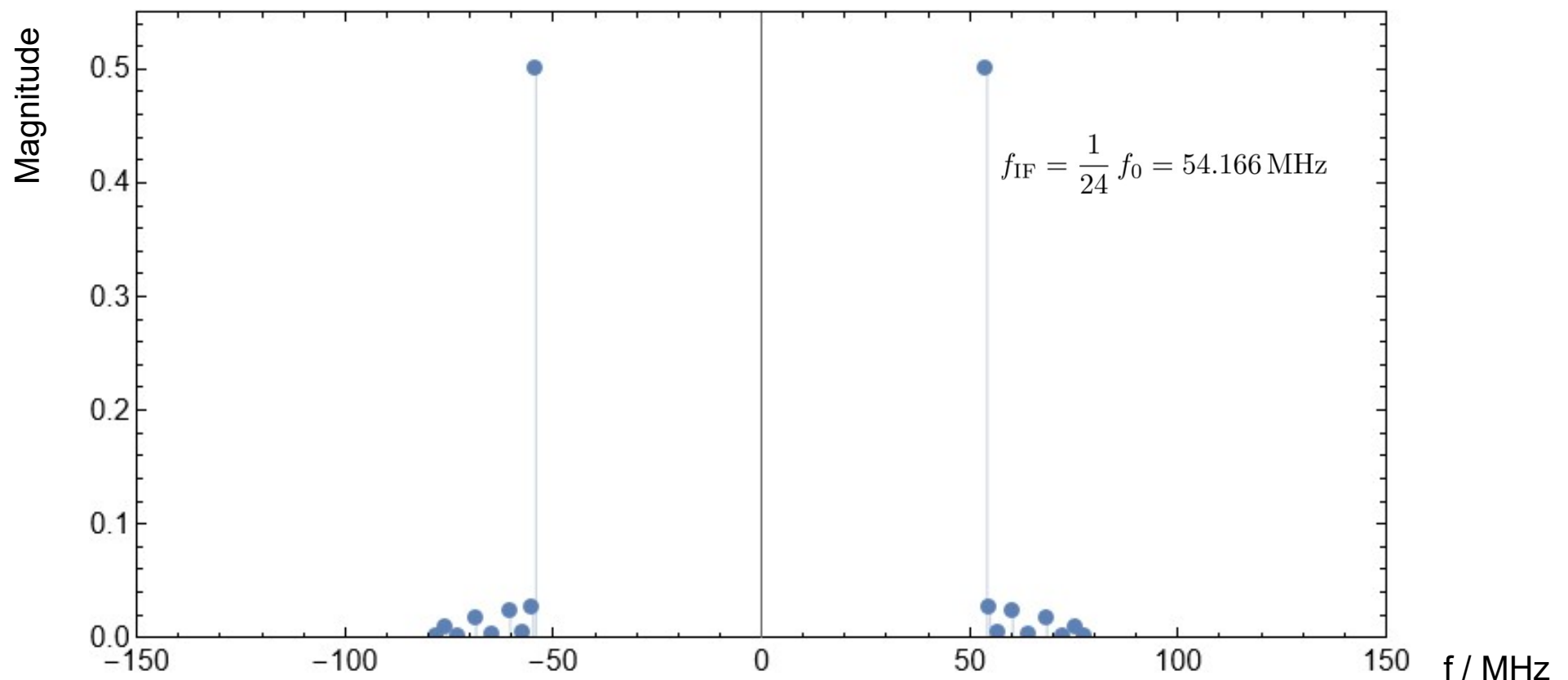


- Spectrum after Point-Charge Excitation
 - First and Second Monopole Passband (after Mixer)



Numerical Results

- Spectrum after Point-Charge Excitation
 - First and Second Monopole Passband (Mixed, Zoom)

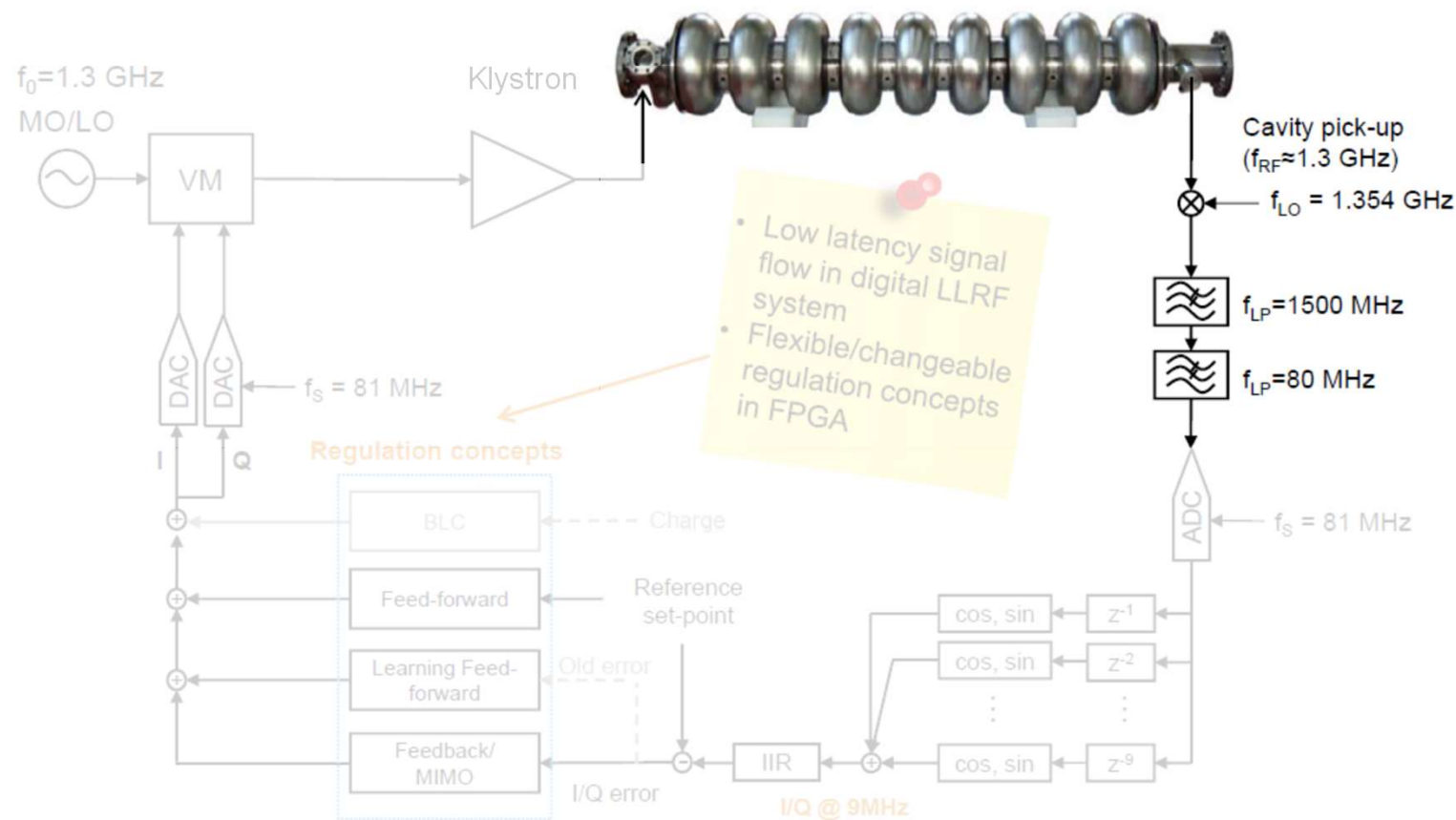


Numerical Results



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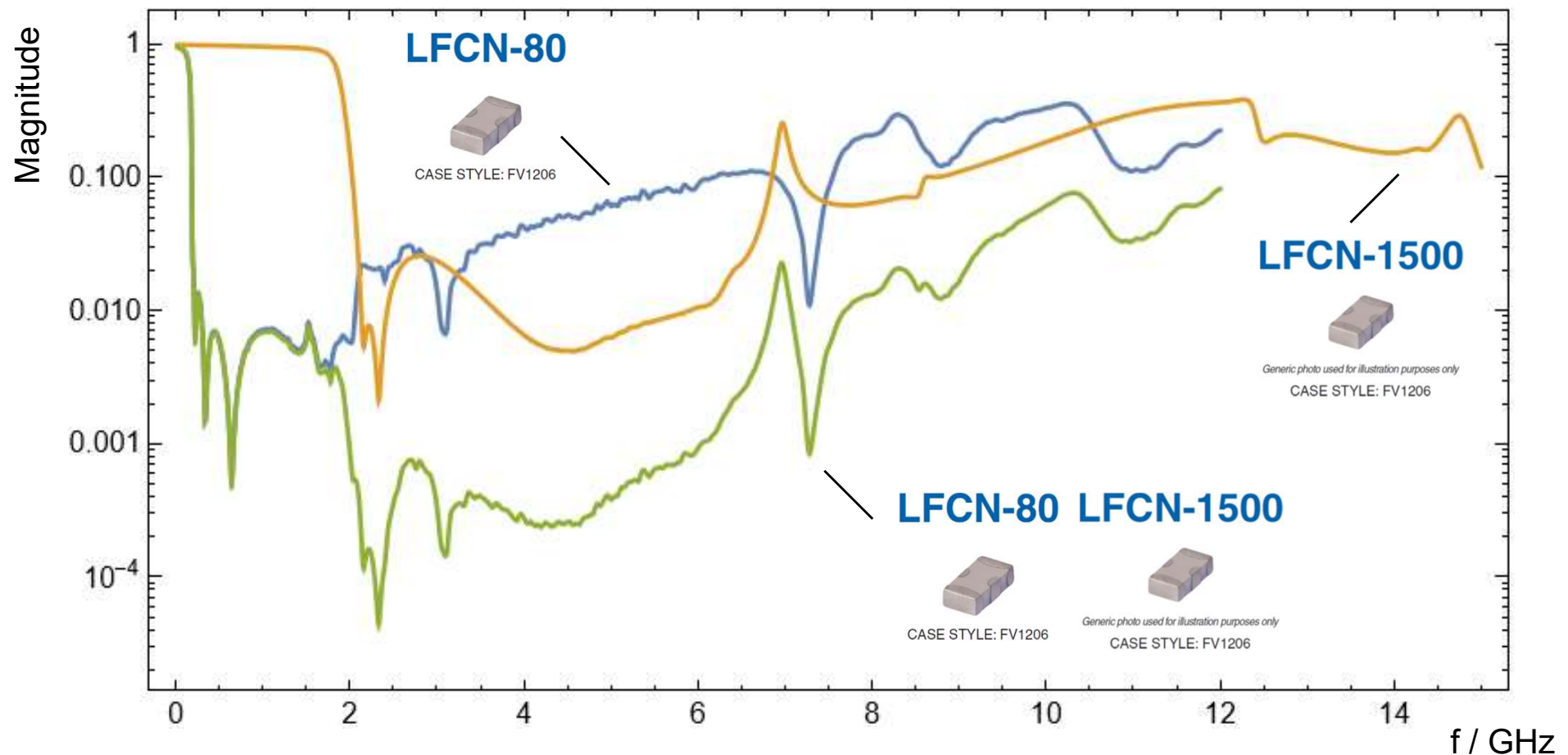
▪ SRF Cavity Regulation



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Numerical Results

▪ Low Pass Filter (Mini-Circuits LFCN-1500 & LFCN-80)

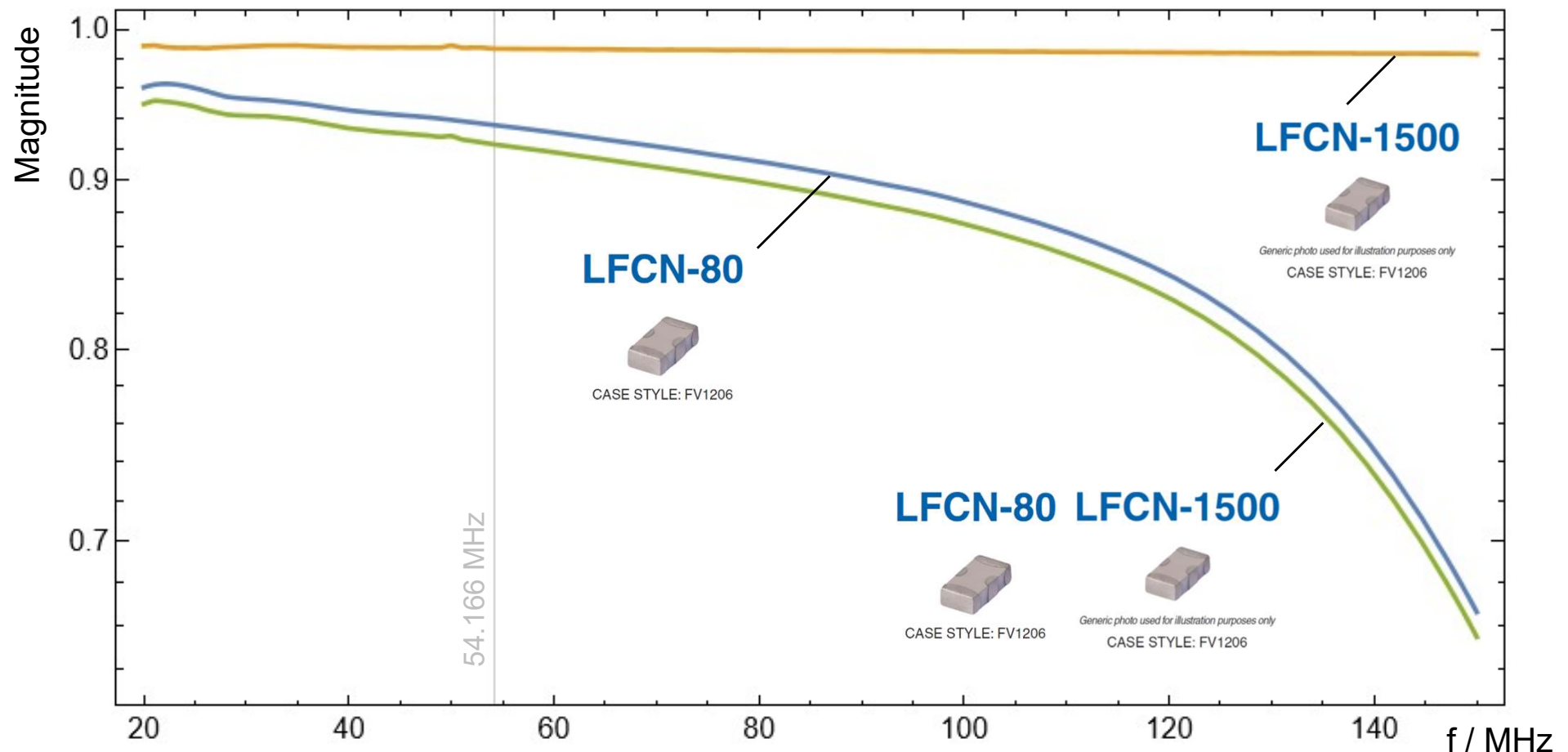


Numerical Results



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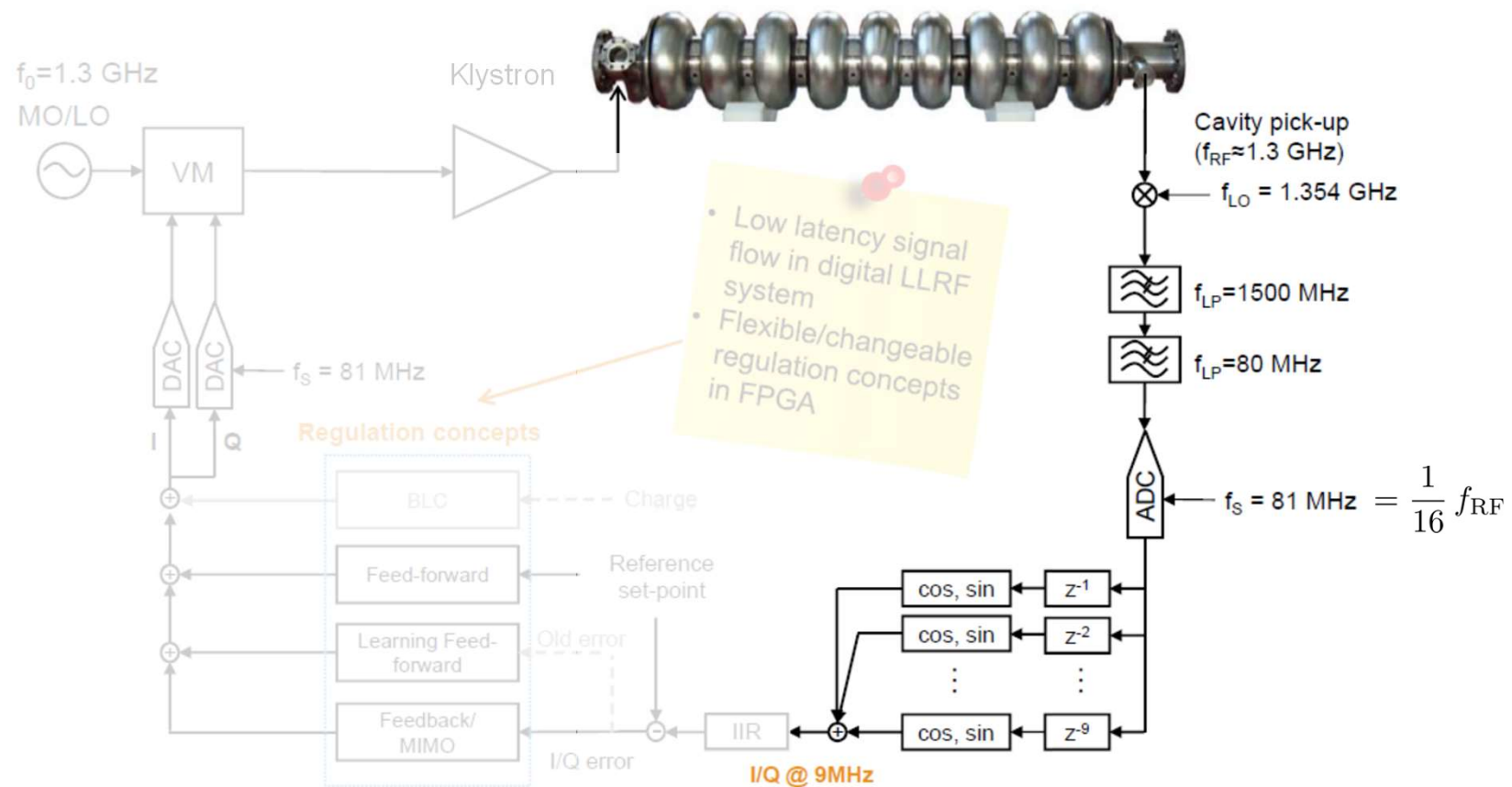
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Numerical Results



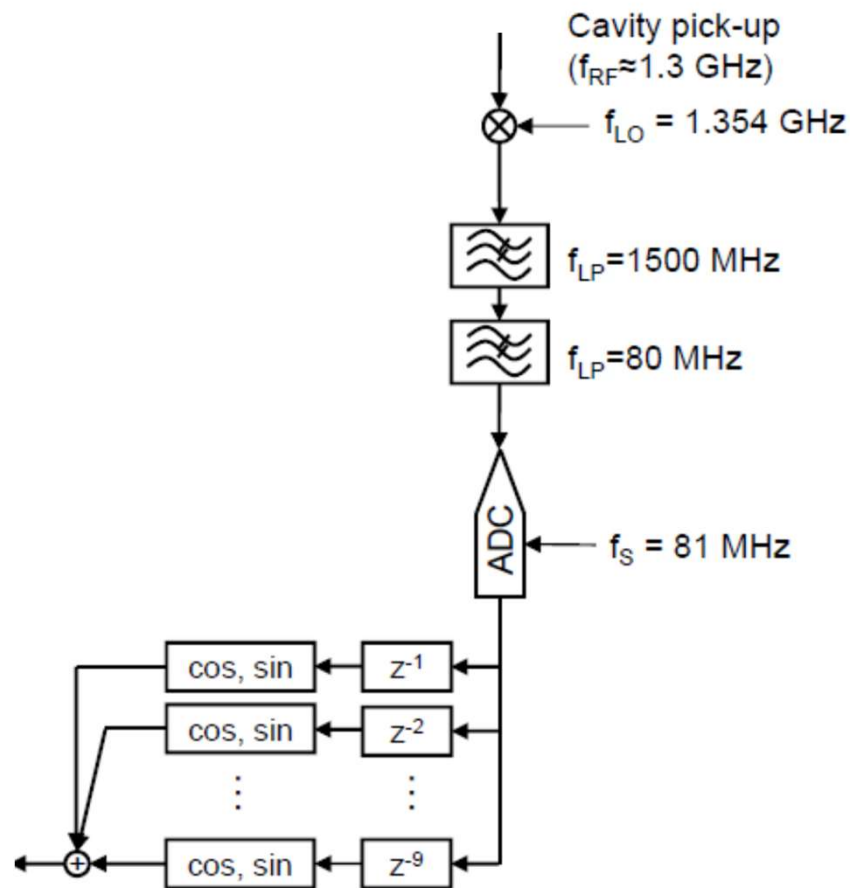
▪ SRF Cavity Regulation



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Numerical Results

▪ Signal-Processing Unit (Digital Fourier Transform)



Mode	Frequency (GHz)	Gain	Excitation
1	1.2764	0.238	0.000
2	1.2784	0.248	0.004
3	1.2816	0.185	0.000
4	1.2856	0.309	0.010
5	1.2898	0.117	0.000
6	1.2938	0.483	0.022
7	1.2971	0.944	0.007
8	1.2993	1.022	0.052
9	1.3000	1.000	1.000
10	2.3786	0.005	0.000
11	2.3835	0.007	0.000
12	2.3913	0.002	0.000
13	2.4016	0.002	0.000
14	2.4137	0.002	0.000
15	2.4265	0.002	0.000
16	2.4386	0.007	0.003
17	2.4482	0.004	0.001
18	2.4539	0.002	0.001

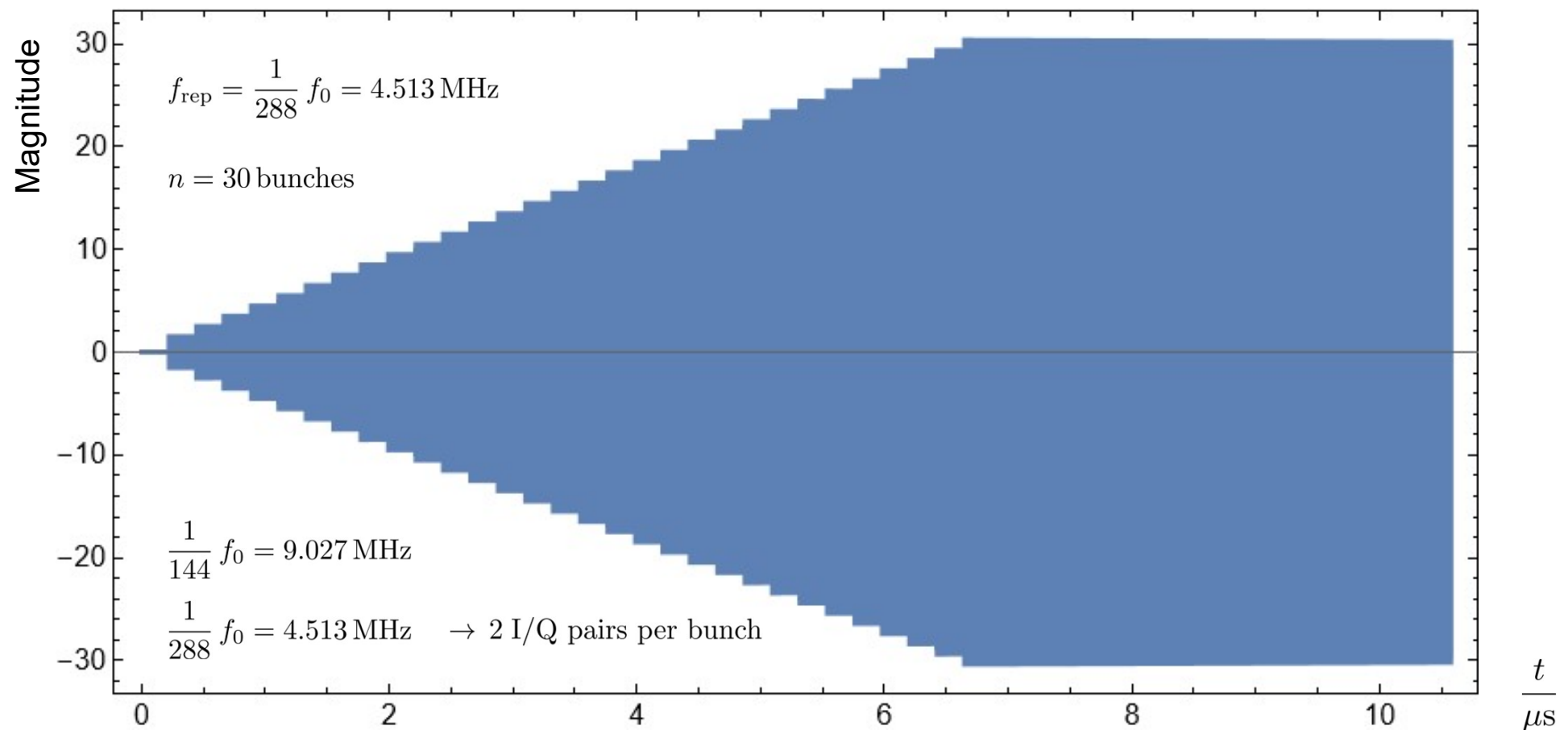
0.095

Numerical Results



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▪ Pulse-Train Excitation

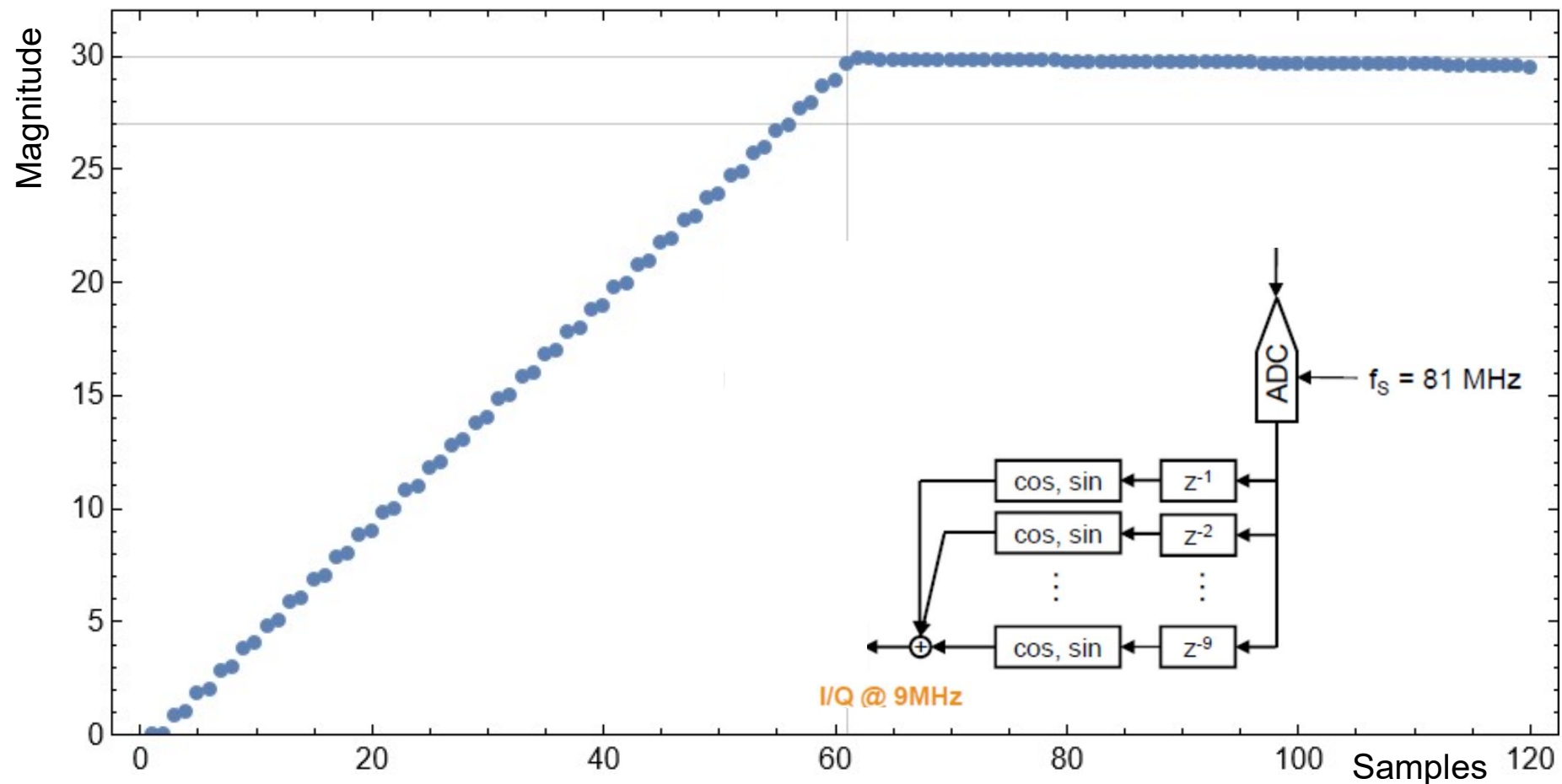


Numerical Results



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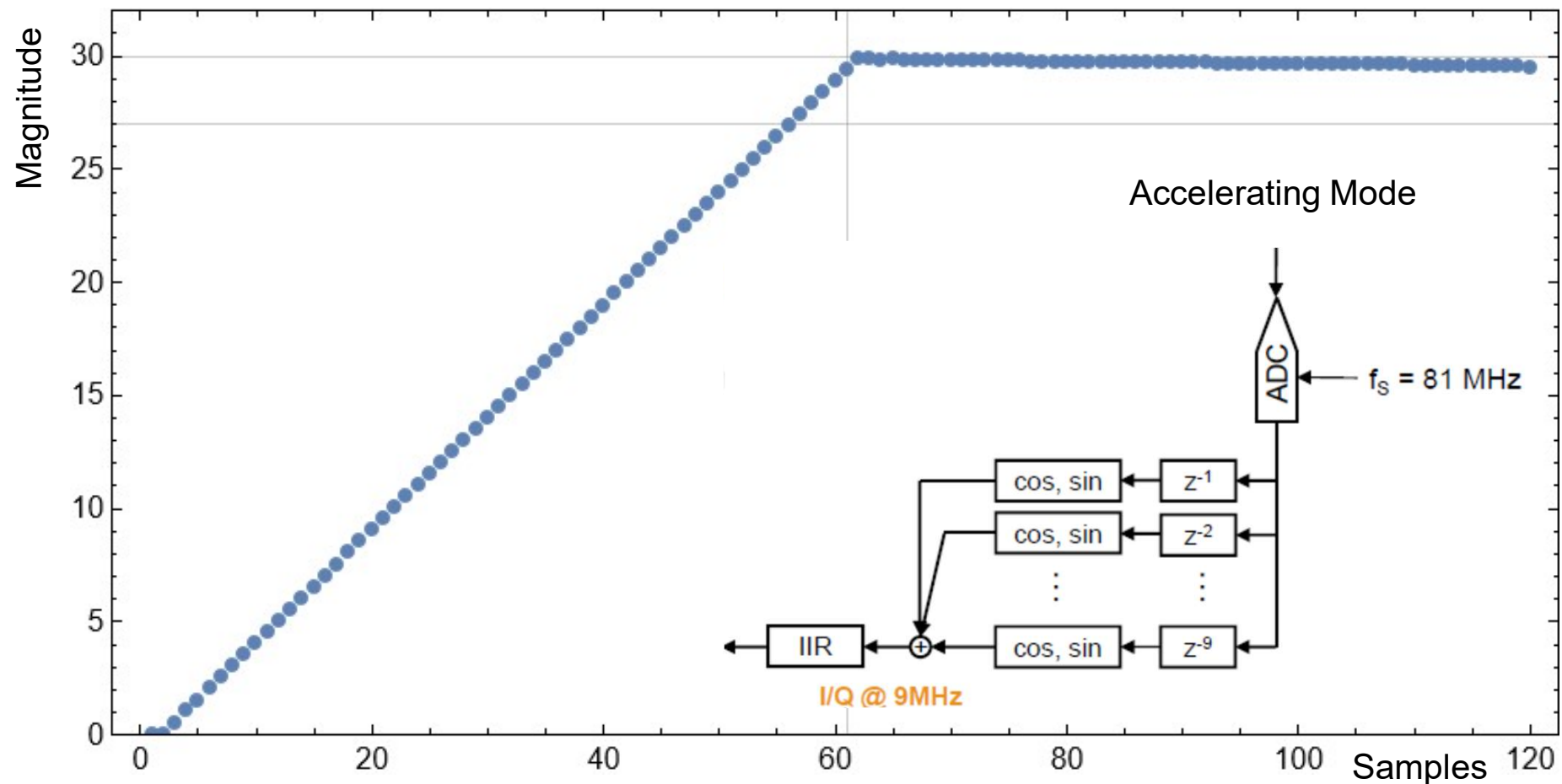


Numerical Results



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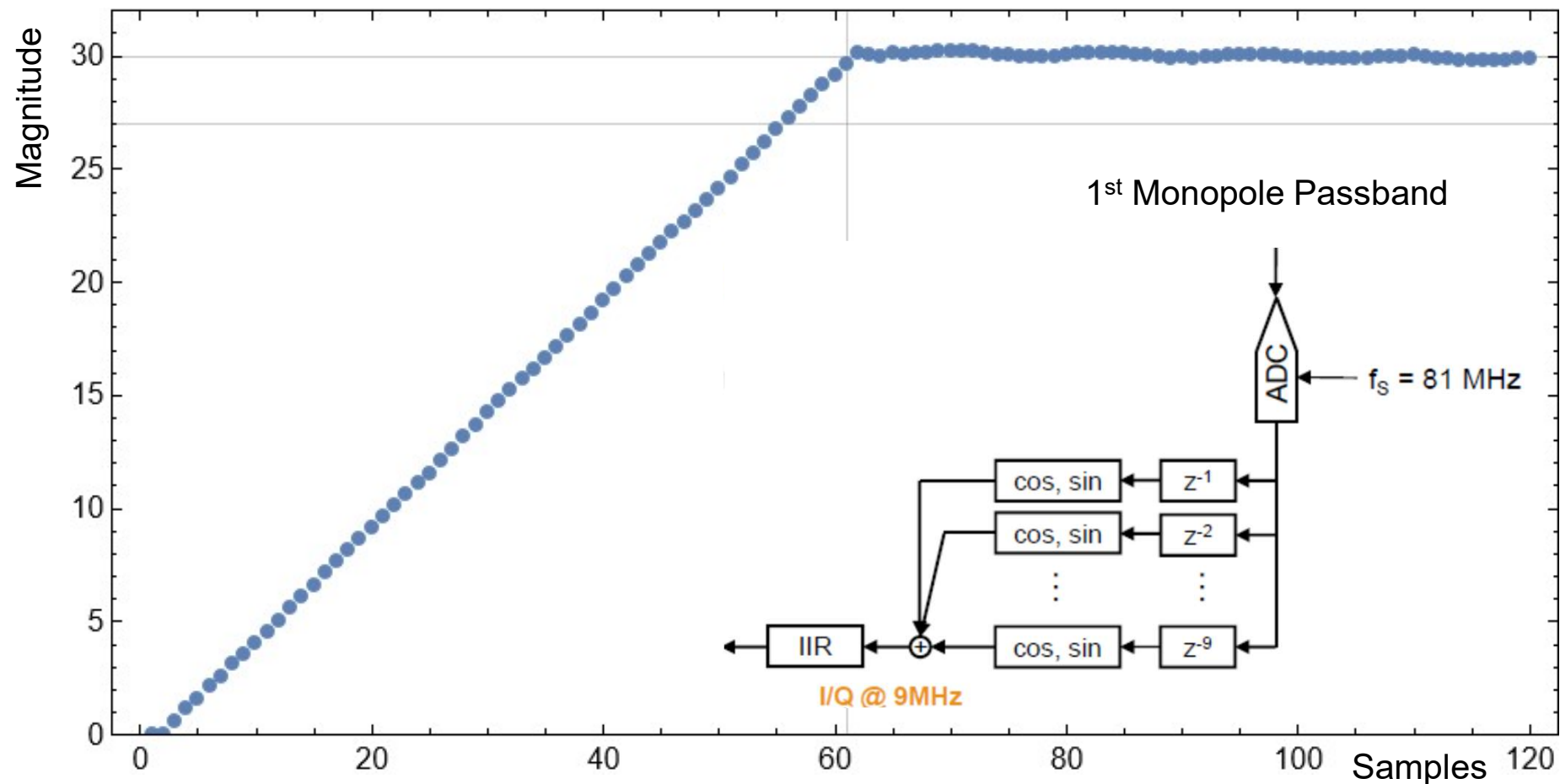


Numerical Results



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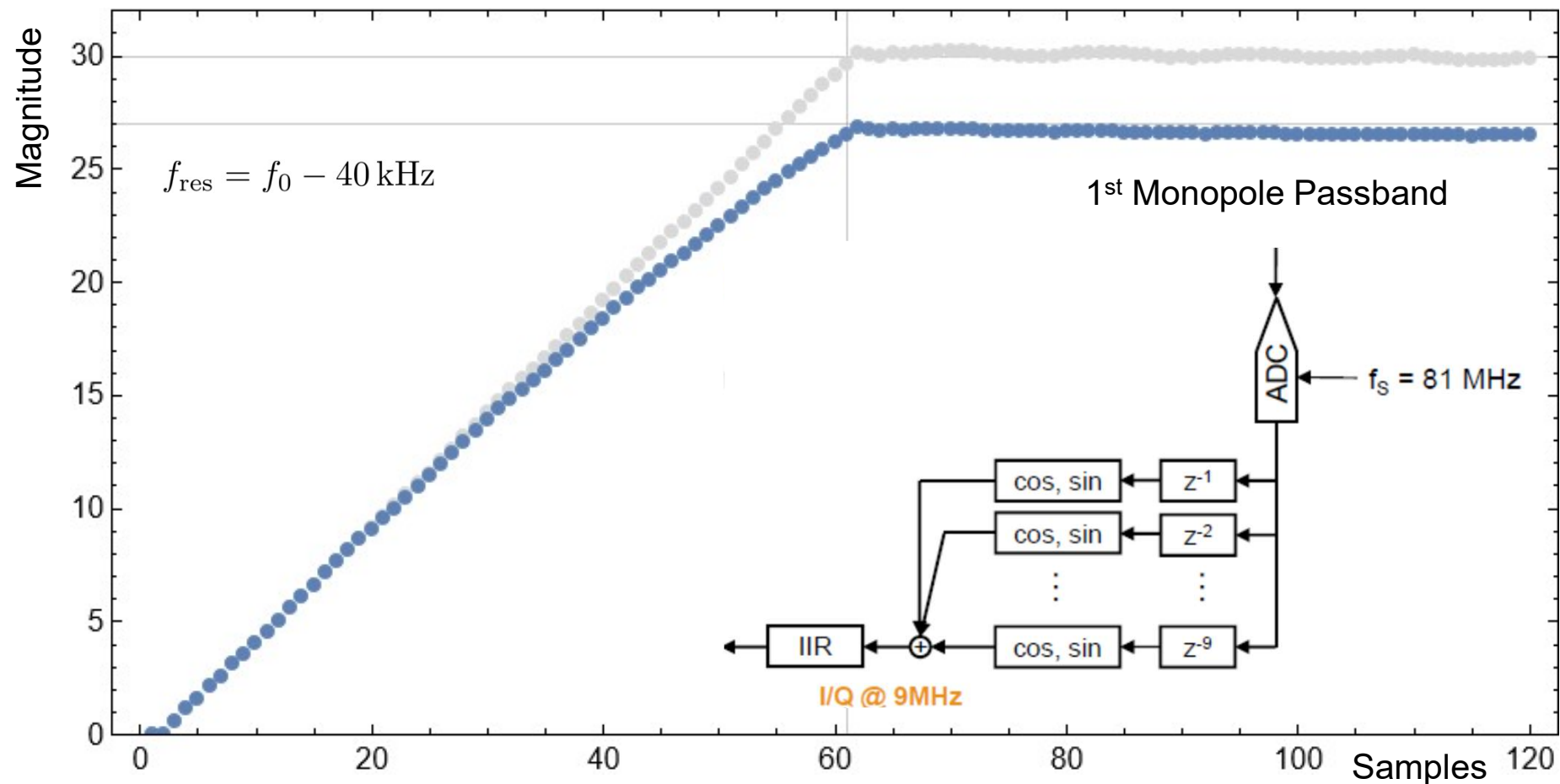


Numerical Results



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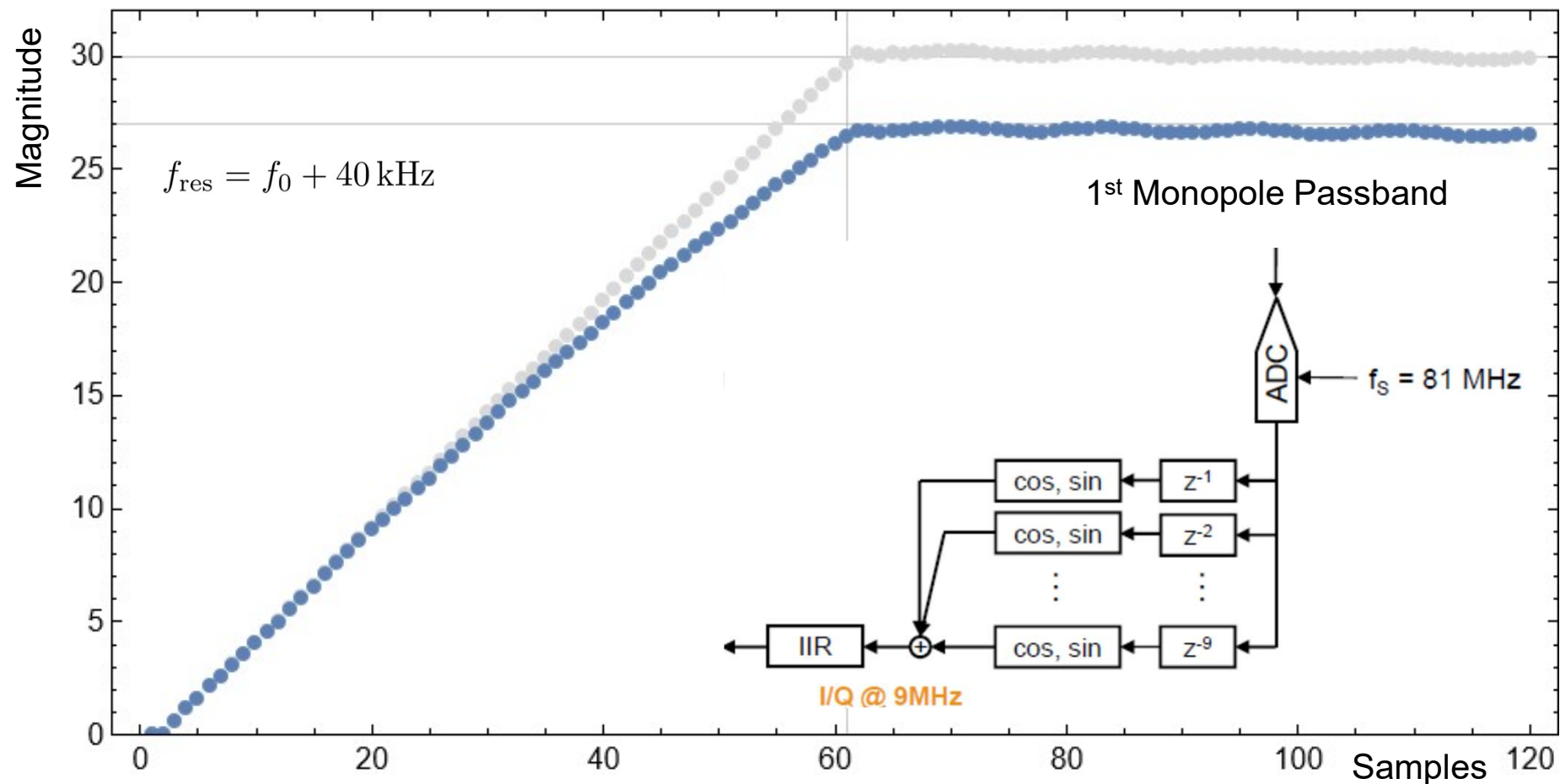


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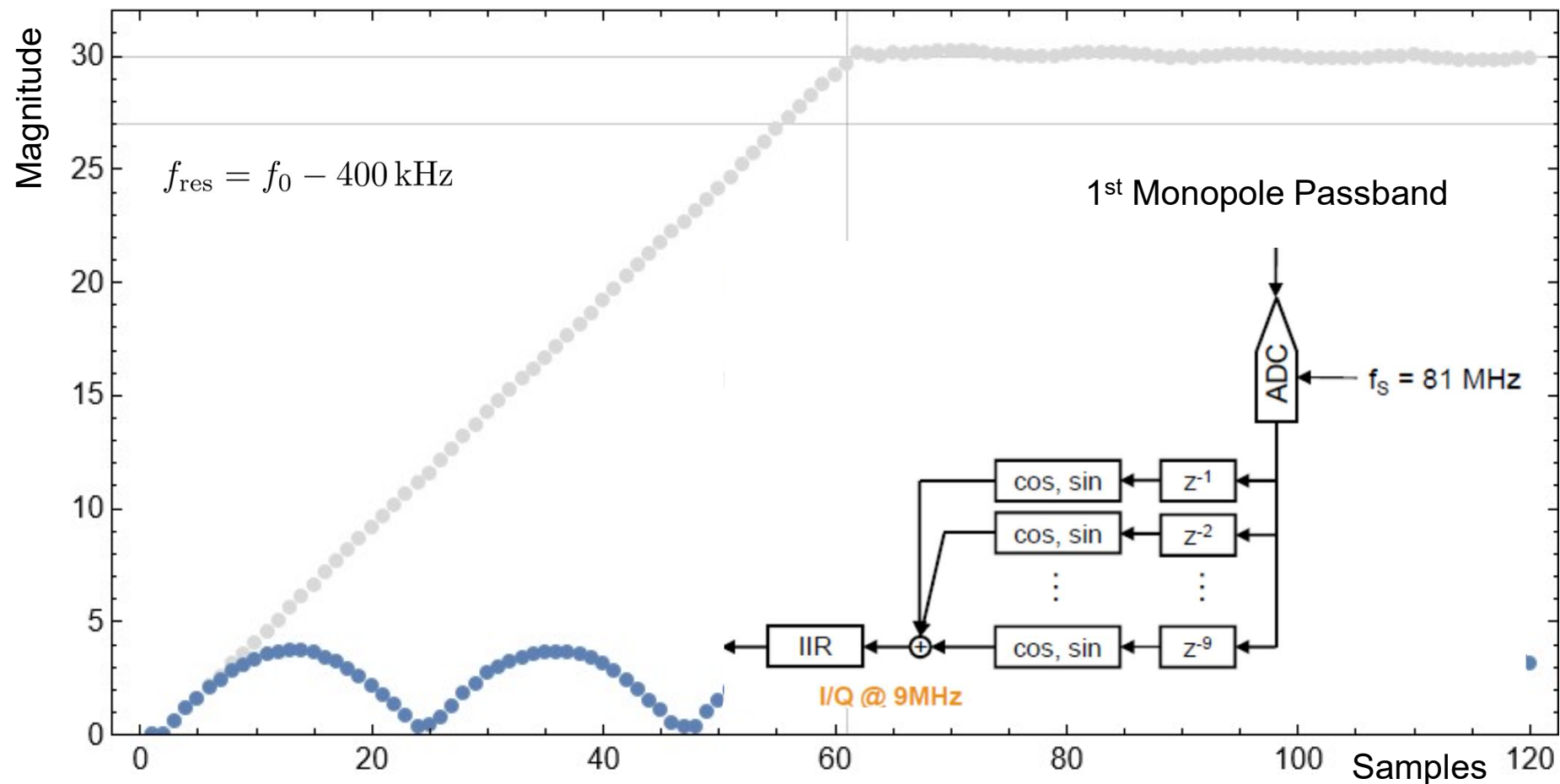


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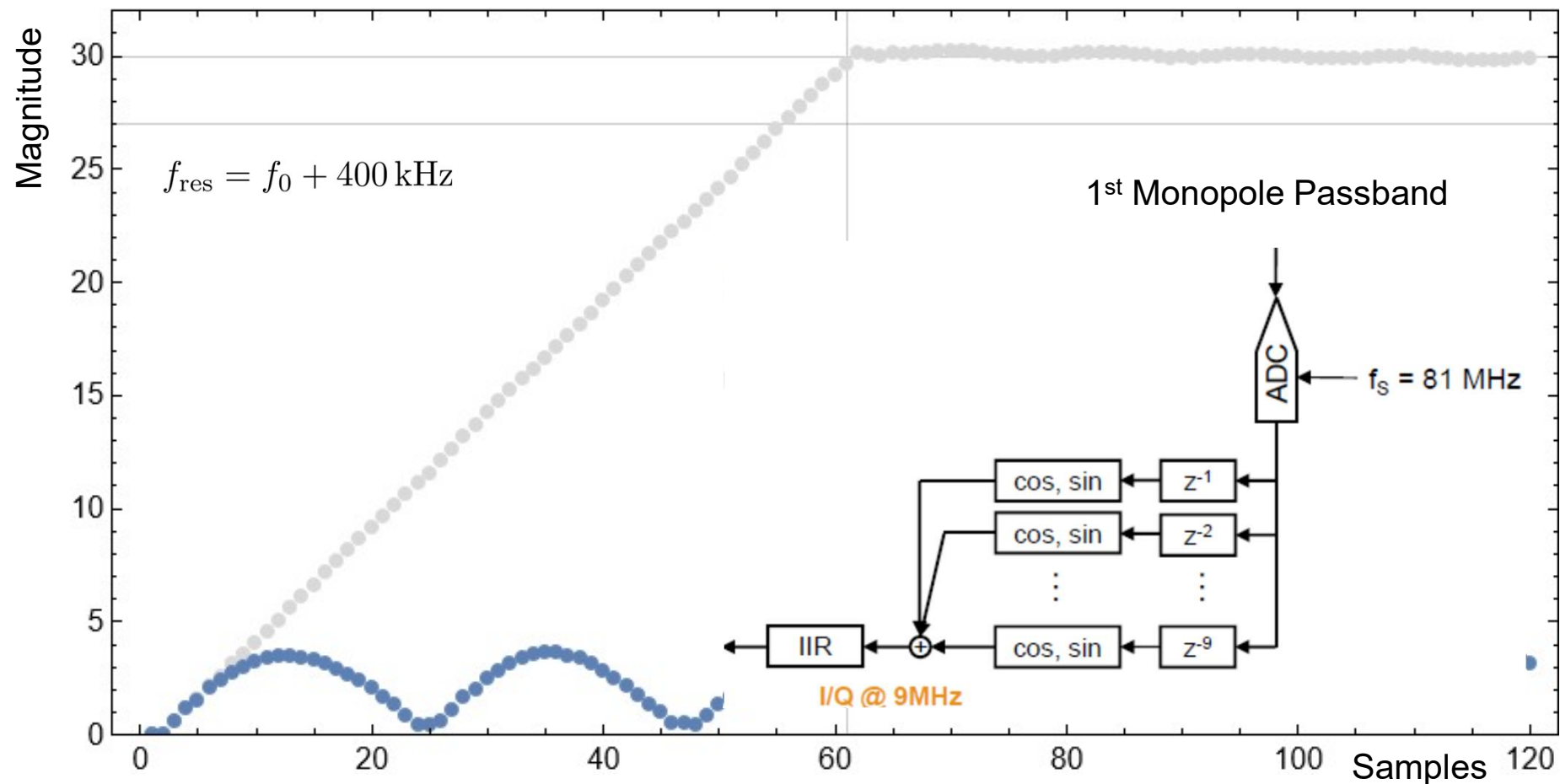


Numerical Results



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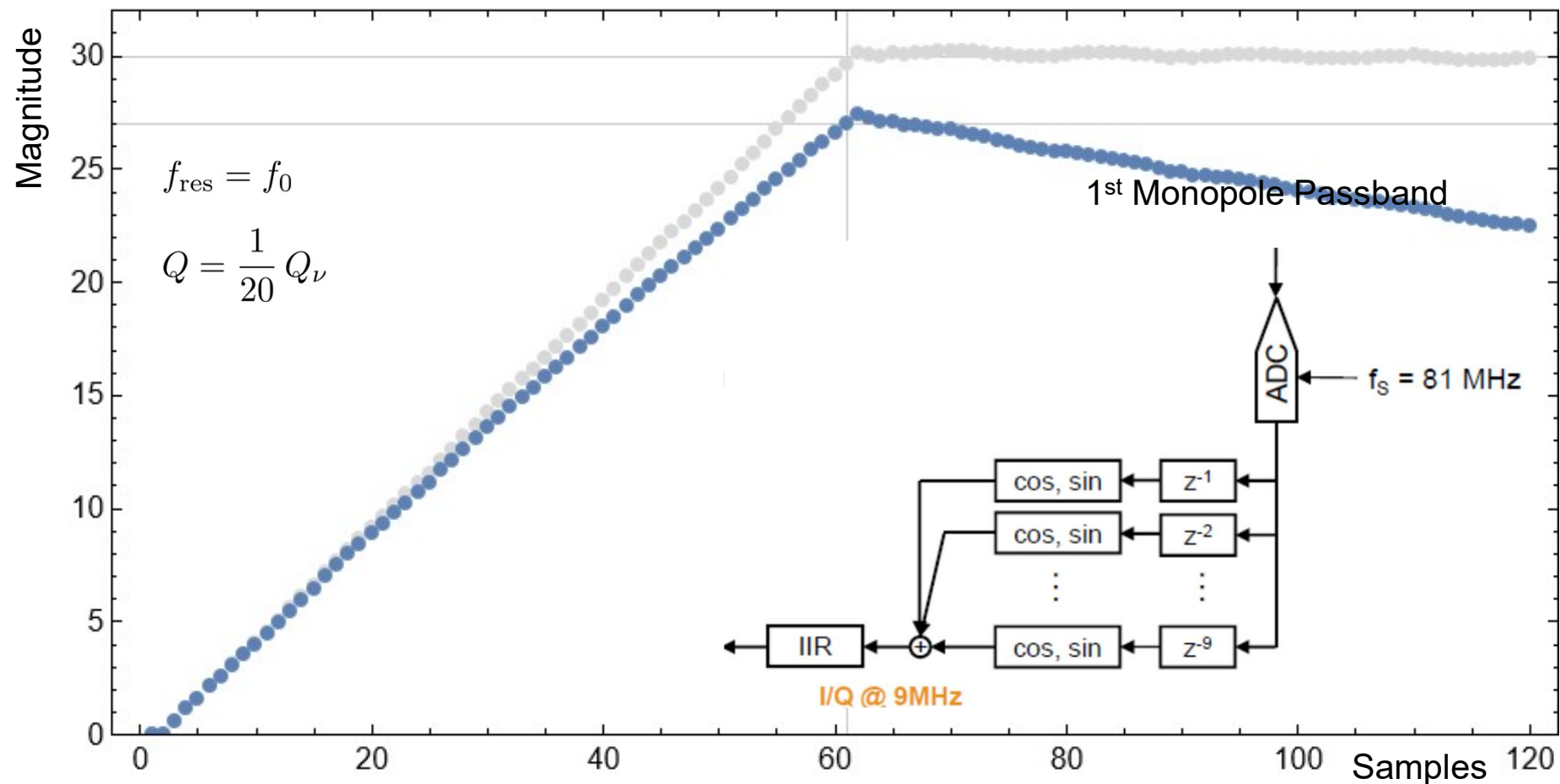


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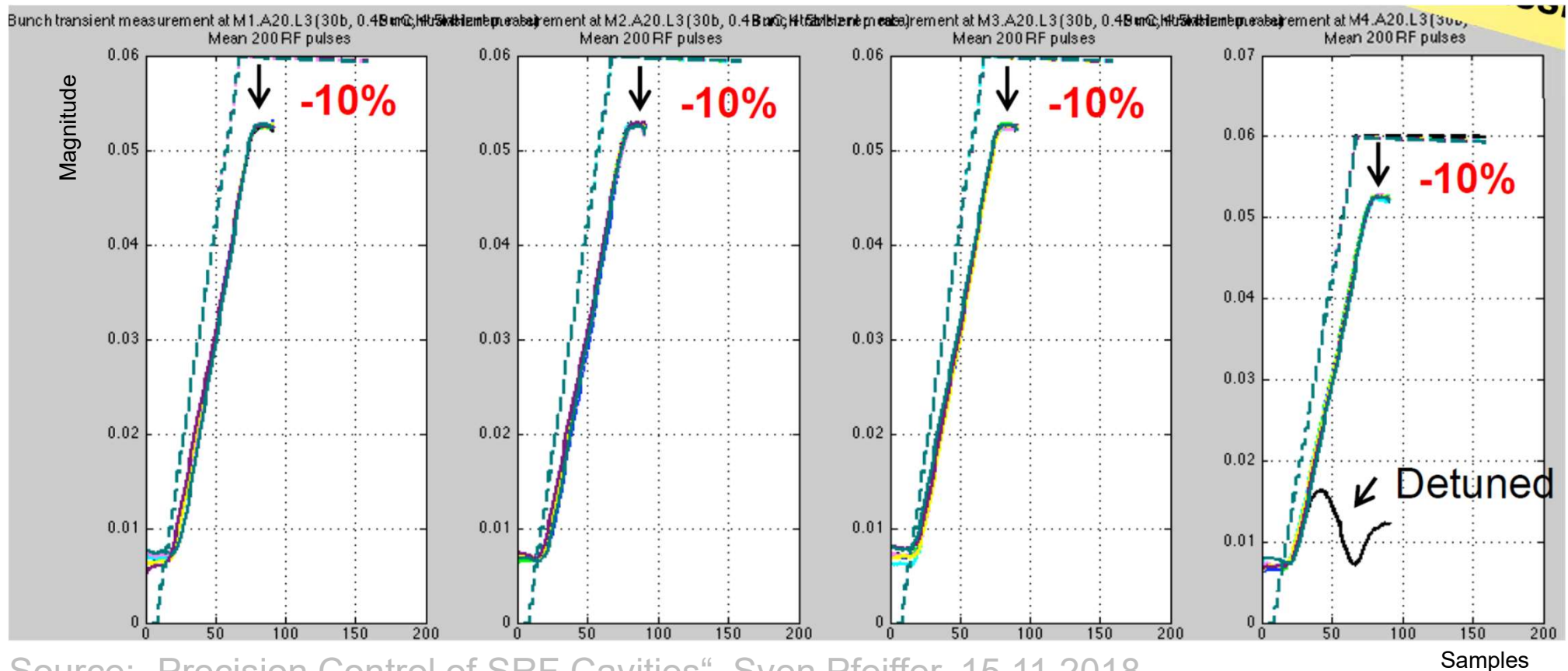
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▪ Summary

- Modeling of the entire signal-processing line
 - Predefined Input Signal
 - Amplitude, Frequency, Phase
 - Single Mode, Multi-Mode
 - Steady State, Single Particle, Multi-Particle
 - Mixing
 - Analog Filtering
 - Analog to Digital Conversion, Sampling
 - Digital Fourier Transform
 - Digital IIR Filter to obtain smooth Amplitude and Phase

■ Summary

- Modeling of the entire signal-processing line



No general design problem recognizable

■ Outlook

- Measurement of the original pickup signal possible?
- Measurement feasible for single-bunch excitation?
- Characterization of the entire signal-processing line by laboratory-based high-frequency signal generator?

