



UPDATED REDUCED MAGNETIC VECTOR POTENTIAL METHOD

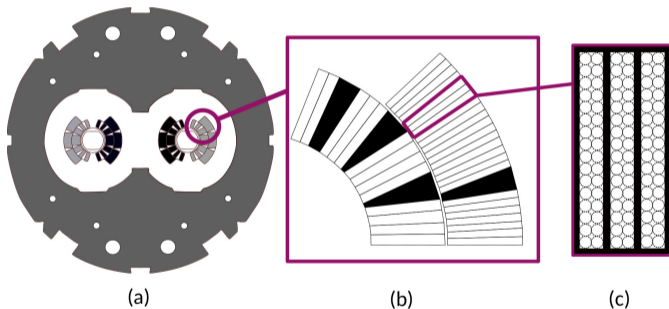
for Superconducting Accelerator Magnets

Laura D'Angelo, Dominik Moll, Herbert De Gersem

Institut für Teilchenbeschleunigung und Elektromagnetische Felder (TEMF)

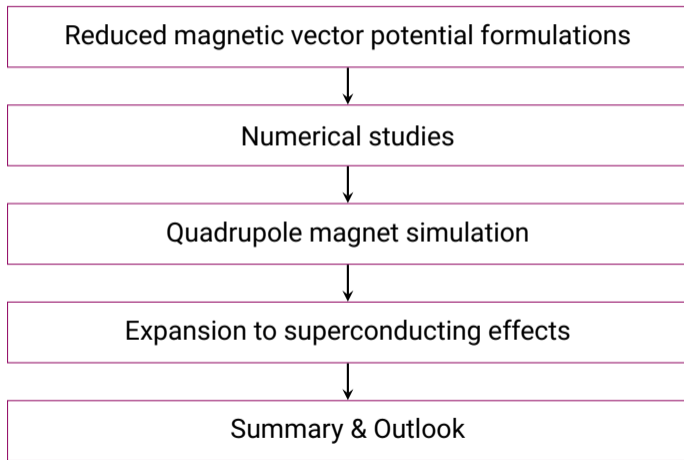
27.06.2024

SUPERCONDUCTING ACCELERATOR MAGNET = MULTI-SCALE PROBLEM

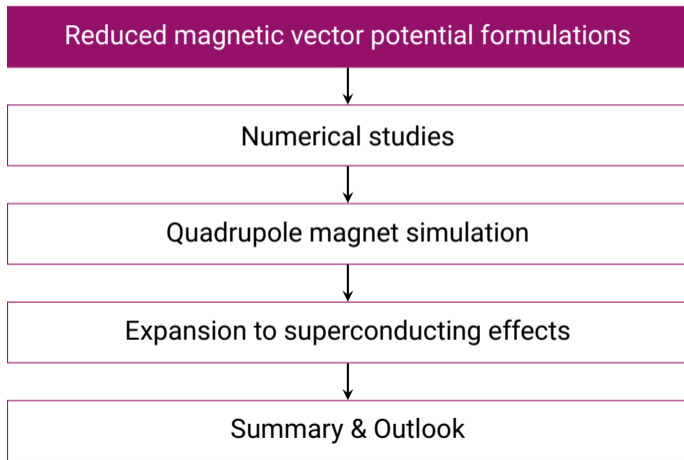


- **Problem:** Meshing all geometrical details within a finite-element method is **too expensive!**
- **Idea:** **Do not resolve** the coils/cables/wires in the FE mesh itself, but as a separate **set of threads** & compute their contribution by **Biot-Savart's law**

OUTLINE



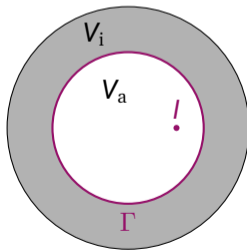
OUTLINE



PHYSICAL PROBLEM

We want to solve:

$$\begin{aligned} \nabla \times (\nu \nabla \times \vec{A}) &= \vec{J} && \text{in } V, \\ \vec{n} \times \vec{A} &= 0 && \text{on } \partial V. \end{aligned}$$



V consists of

- V_a : air domain with source currents
- V_i : source-free domain, typically iron yoke
- Γ : interface surface between V_a and V_i

REDUCED MAGNETIC VECTOR POTENTIAL (RMVP) ANSATZ

Split the magnetic vector potential (MVP):

$$\vec{A}(\vec{r}, t) = \underbrace{\vec{A}_s(\vec{r})}_{\text{source MVP}} + \underbrace{\vec{A}_r(\vec{r})}_{\text{reduced MVP}}$$

Compute a **Biot-Savart** integral for each thread \mathcal{L}' :

$$\vec{A}_s(\vec{r}) = \frac{\mu_0}{4\pi} \int_{\mathcal{L}'} \frac{I}{|\vec{r} - \vec{r}'|} d\vec{r}'$$

Compute \vec{A}_r using the finite-element method:

$$\vec{A}_r(\vec{r}) \approx \sum_{j=1}^{N_{\text{edge}}} \hat{a}_{s,j} \vec{w}_j(\vec{r})$$

STANDARD RMVP FORMULATION

CHRISTIAN PAUL 1997

1. Evaluate the **source MVP** \vec{A}_s via Biot-Savart for each point $\vec{r} \in V$.

2. Find the **reduced MVP** $\vec{A}_r \in H_r(\text{curl}; V) = \left\{ \vec{A}_r \in H(\text{curl}; V) : \vec{n} \times \vec{A}_r = -\vec{n} \times \vec{A}_s \text{ on } \partial V \right\}$, s.t.

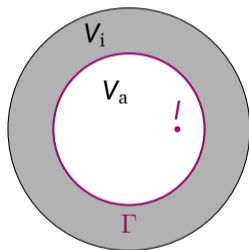
$$\left(\nu \nabla \times \vec{A}_r, \nabla \times \vec{A}'_r \right)_V = - \left(\nu \nabla \times \vec{A}_s, \nabla \times \vec{A}'_r \right)_{V_i} \quad \forall \vec{A}'_r \in H_r(\text{curl}; V)$$

3. Compose total MVP: $\vec{A} = \vec{A}_s + \vec{A}_r$ in V .

→ Can get computationally **expensive!**

UPDATED RMVP FORMULATION: DERIVATION

D'ANGELO ET AL. 2024



Goal: Have \vec{A}_s only in V_a .

Express the boundary value problem for V_a and V_i separately and introduce the source MVP \vec{A}_s in V_a :

$$\nabla \times \left(\nu_0 \nabla \times \left(\vec{A}_a - \vec{A}_s \right) \right) = 0 \quad \text{in } V_a,$$

$$\nabla \times \left(\nu \nabla \times \vec{A}_i \right) = 0 \quad \text{in } V_i,$$

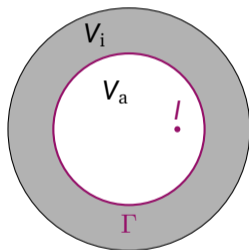
$$\vec{n} \times \vec{A}_a = \vec{n} \times \vec{A}_i \quad \text{at } \Gamma,$$

$$\vec{n} \times \vec{H}_a = \vec{n} \times \vec{H}_i \quad \text{at } \Gamma,$$

$$\vec{n} \times \vec{A}_i = 0 \quad \text{at } \partial V.$$

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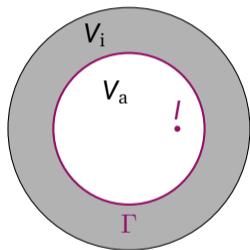
$$\vec{n} \times \vec{H}_a = \vec{n} \times \vec{H}_i \quad \text{at } \Gamma,$$

$$\vec{n} \times \vec{A}_i = 0 \quad \text{at } \partial V.$$

→ **Problem:** The separate solutions $\vec{A}_a - \vec{A}_s$ in V_a and \vec{A}_i in V_i are **not continuous** at Γ !

UPDATED RMVP FORMULATION: DERIVATION

D'ANGELO ET AL. 2024



Solution: Enforce continuity by introducing the **image MVP** \vec{A}_m with $\vec{n} \times \vec{A}_m = -\vec{n} \times \vec{A}_s$ on Γ ,

$$\nabla \times \left(\nu_0 \nabla \times (\vec{A}_a - \vec{A}_s - \vec{A}_m) \right) = 0 \quad \text{in } V_a,$$

$$\nabla \times \left(\nu \nabla \times \vec{A}_i \right) = 0 \quad \text{in } V_i,$$

$$\vec{n} \times \vec{A}_a = \vec{n} \times \vec{A}_i \quad \text{at } \Gamma,$$

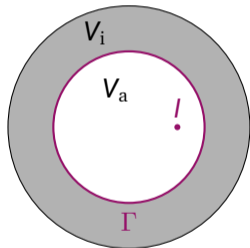
$$\vec{n} \times \vec{H}_a = \vec{n} \times \vec{H}_i \quad \text{at } \Gamma,$$

$$\vec{n} \times \vec{A}_i = 0 \quad \text{at } \partial V.$$

UPDATED RMVP FORMULATION: DERIVATION

D'ANGELO ET AL. 2024

Solution: Enforce continuity by introducing the **image MVP** \vec{A}_m with $\vec{n} \times \vec{A}_m = -\vec{n} \times \vec{A}_s$ on Γ , **and add zero:**



$$\nabla \times (\nu_0 \nabla \times (\vec{A}_a - \vec{A}_s - \vec{A}_m)) = 0 \quad \text{in } V_a,$$

$$\nabla \times (\nu \nabla \times \vec{A}_i) = 0 \quad \text{in } V_i,$$

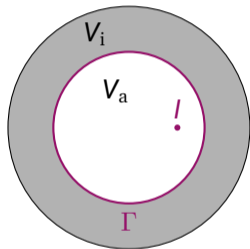
$$\vec{n} \times \vec{A}_a - \underbrace{\vec{n} \times (\vec{A}_s + \vec{A}_m)}_{=0} = \vec{n} \times \vec{A}_i \quad \text{at } \Gamma,$$

$$\vec{n} \times \vec{H}_a - \underbrace{\vec{n} \times (\vec{H}_s + \vec{H}_m) + \vec{n} \times (\vec{H}_s + \vec{H}_m)}_{=0} = \vec{n} \times \vec{H}_i \quad \text{at } \Gamma,$$

$$\vec{n} \times \vec{A}_i = 0 \quad \text{at } \partial V.$$

UPDATED RMVP FORMULATION: DERIVATION

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 Summarize with $\vec{A}'_a = \vec{A}_a - \vec{A}_s - \vec{A}_m$:

$$\nabla \times (\nu_0 \nabla \times \vec{A}'_a) = 0 \quad \text{in } V_a,$$

$$\nabla \times (\nu \nabla \times \vec{A}_i) = 0 \quad \text{in } V_i,$$

$$\vec{n} \times \vec{A}'_a = \vec{n} \times \vec{A}_i \quad \text{at } \Gamma,$$

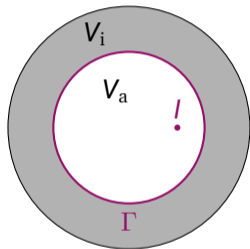
$$\vec{n} \times \vec{H}'_a - \vec{n} \times \vec{H}_i = \vec{n} \times (\vec{H}_s + \vec{H}_m) \quad \text{at } \Gamma,$$

$$\vec{n} \times \vec{A}_i = 0 \quad \text{at } \partial V.$$

- Sub-domain solutions \vec{A}'_a and \vec{A}_i are tangentially continuous at Γ .
- Jump of \vec{H} can be interpreted as a surface current density $\vec{K}_g = \vec{n} \times (\vec{H}_s + \vec{H}_m)$.

UPDATED RMVP FORMULATION: DERIVATION

D'ANGELO ET AL. 2024


 Summarize with $\vec{A}'_a = \vec{A}_a - \vec{A}_s - \vec{A}_m$:

$$\nabla \times (\nu_0 \nabla \times \vec{A}_g) = 0 \quad \text{in } V_a,$$

$$\nabla \times (\nu \nabla \times \vec{A}_g) = 0 \quad \text{in } V_i,$$

$$\vec{n} \times \vec{A}_g = \vec{n} \times \vec{A}_g \quad \text{at } \Gamma,$$

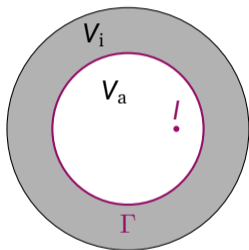
$$\vec{n} \times \vec{H}_g - \vec{n} \times \vec{H}_g = \vec{n} \times (\vec{H}_s + \vec{H}_m) \quad \text{at } \Gamma,$$

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UPDATED RMVP FORMULATION: DERIVATION

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Finally, substitute

$$\vec{A}_g = \begin{cases} \vec{A}'_a & \text{in } V_a, \\ \vec{A}_i & \text{in } V_i, \end{cases}$$

to obtain a single domain problem:

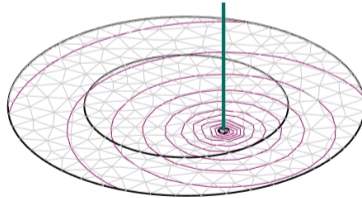
$$\begin{aligned} \nabla \times (\nu \nabla \times \vec{A}_g) &= \vec{K}_g \delta_\Gamma && \text{in } V, \\ \vec{n} \times \vec{A}_g &= 0 && \text{at } \partial V. \end{aligned}$$

UPDATED RMVP FORMULATION: RECIPE

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1. Evaluate the **source MVP \vec{A}_s** via Biot-Savart **only at the interface $\Gamma = \partial V_a$** ...
...and on every point of interest $\vec{r} \in V_a$.

→ Huge improvement in computational efficiency!



source MVP \vec{A}_s (everywhere) and **source current**

UPDATED RMVP FORMULATION: RECIPE

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2. Find the **image MVP** $\vec{A}_m \in H(\text{curl}; V_a)$, $\vec{n} \times \vec{H}_m \in H^{-1/2}(\text{curl}; \Gamma)$, s.t.

$$\begin{aligned} \left(\nu_0 \nabla \times \vec{A}_m, \nabla \times \vec{A}'_m \right)_{V_a} + \left(\vec{n} \times \vec{H}_m, \vec{A}'_m \right)_{\Gamma} &= 0 & \forall \vec{A}'_m \in H(\text{curl}; V_a), \\ \left(\vec{A}_m, \vec{n} \times \vec{H}'_m \right)_{\Gamma} + \left(\vec{A}_s, \vec{n} \times \vec{H}'_m \right)_{\Gamma} &= 0 & \forall \vec{n} \times \vec{H}'_m \in H^{-1/2}(\text{curl}; \Gamma). \end{aligned}$$

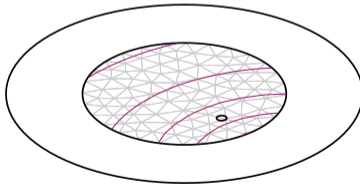


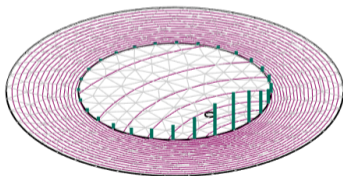
image MVP \vec{A}_m in V_a

UPDATED RMVP FORMULATION: RECIPE

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3. Find the **reaction MVP** $\vec{A}_g \in H_0(\text{curl}; V)$ s.t.

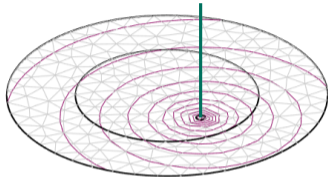
$$\left(\nu \nabla \times \vec{A}_g, \nabla \times \vec{A}'_g \right)_V = \left(\vec{n} \times \vec{H}_s, \vec{A}'_g \right)_\Gamma + \left(\vec{n} \times \vec{H}_m, \vec{A}'_g \right)_\Gamma \quad \forall \vec{A}'_g \in H_0(\text{curl}; V).$$



reaction MVP \vec{A}_g in V ,
surface current density $\vec{K}_g = \vec{n} \times (\vec{H}_s + \vec{H}_m)$ on Γ

UPDATED RMVP FORMULATION: RECIPE

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source MVP \vec{A}_s

+

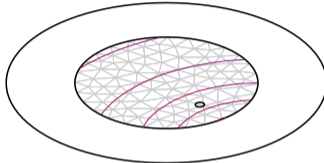
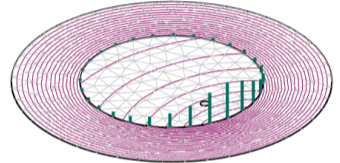


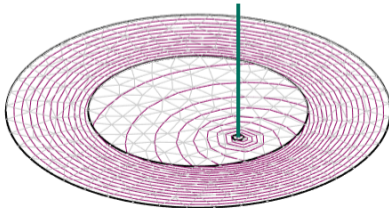
image MVP \vec{A}_m

+



reaction MVP \vec{A}_g

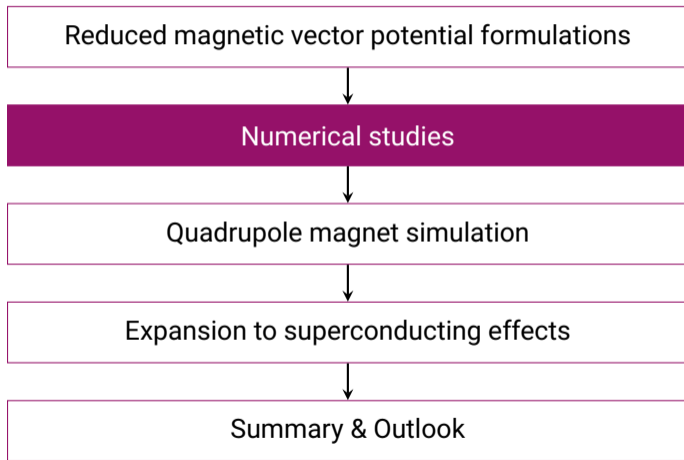
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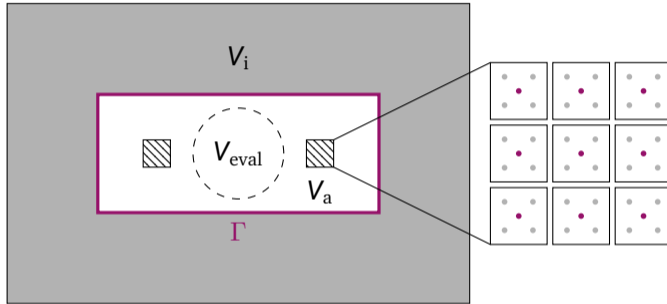
4. Compose final solution:

$$\begin{aligned} \vec{A} &= \vec{A}_s + \vec{A}_m + \vec{A}_g && \text{in } V_a, \\ \vec{A} &= \vec{A}_g && \text{in } V_i. \end{aligned}$$

OUTLINE



RACETRACK COIL MODEL



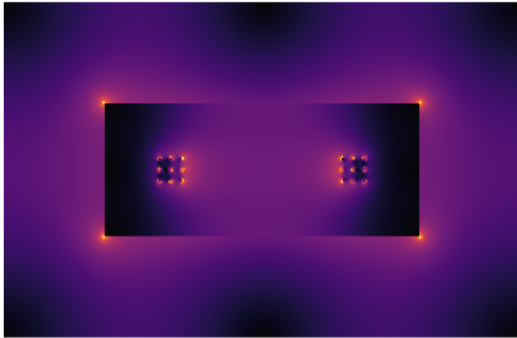
- Discretization of windings as set of **line currents**
- Simplest case: single line currents at **center points**

- Implementation of the RMVP formulation in the open-source FE solver **GetDP**
- 2D linear magnetostatic simulation

MAGNETIC FLUX DENSITY & L²-ERROR

Biot-Savart:

$$\vec{A}_s(\vec{r}) = \frac{\mu_0}{4\pi} \int_{\mathcal{L}'} \frac{I}{|\vec{r} - \vec{r}'|} d\vec{r}'$$



Magnetic flux density magnitude (T)

0.0001

0.55

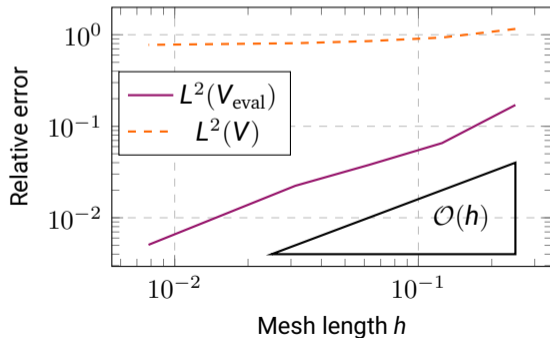
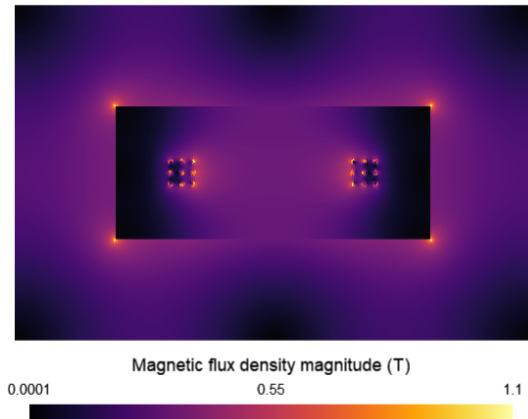
1.1



MAGNETIC FLUX DENSITY & L²-ERROR

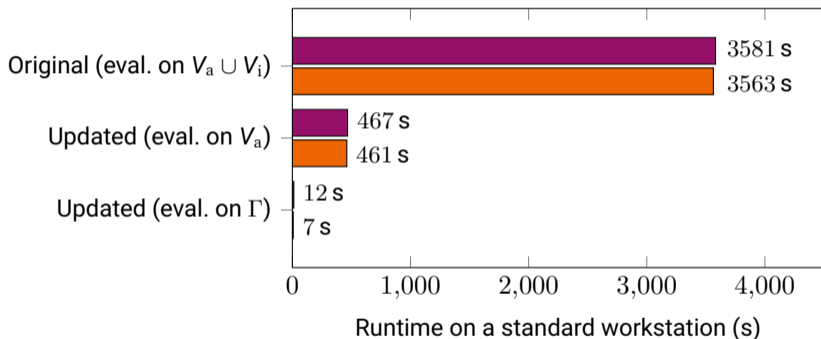
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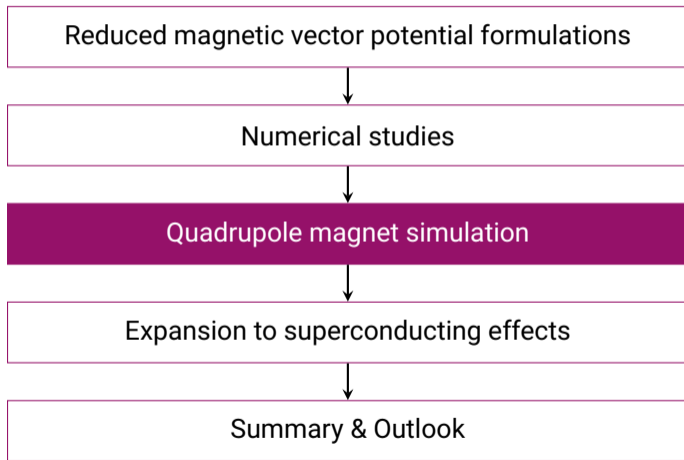
PERFORMANCE COMPARISON

BENCHMARK MODEL WITH > 100,000 DOF AND 18 WIRES

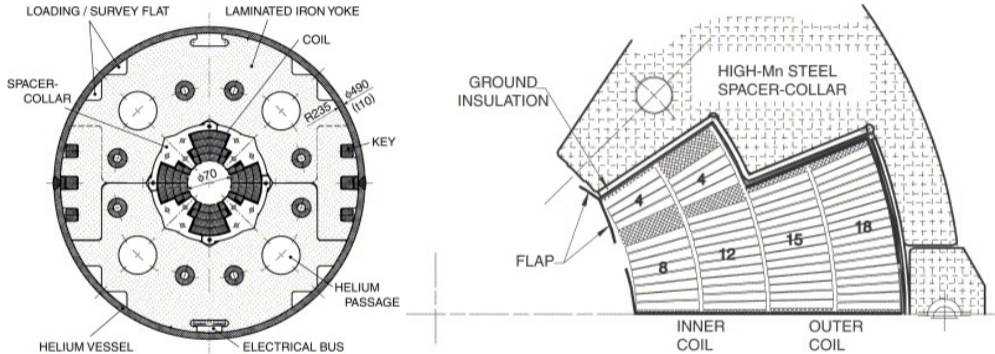


1. **Biot-Savart** computation is dominant \Rightarrow **Parallelize** and use **fast-multipole methods**
2. **Updated RMVP** formulation **by far superior** than standard one

OUTLINE

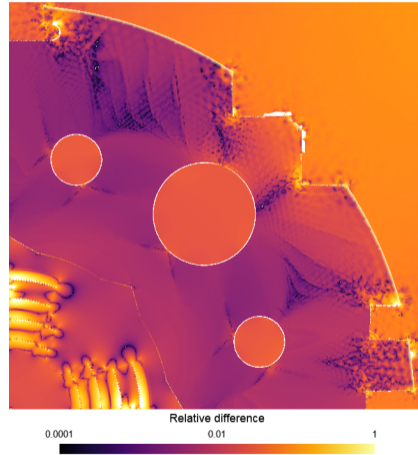
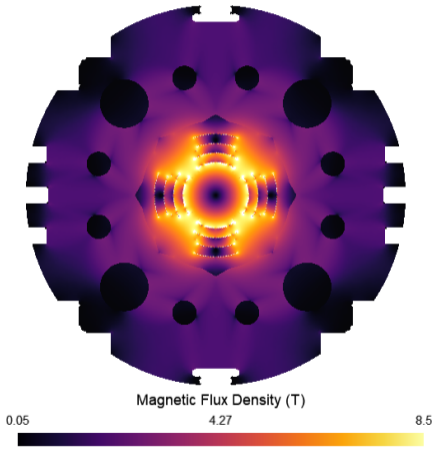


QUADRUPOLE MAGNET: SETUP

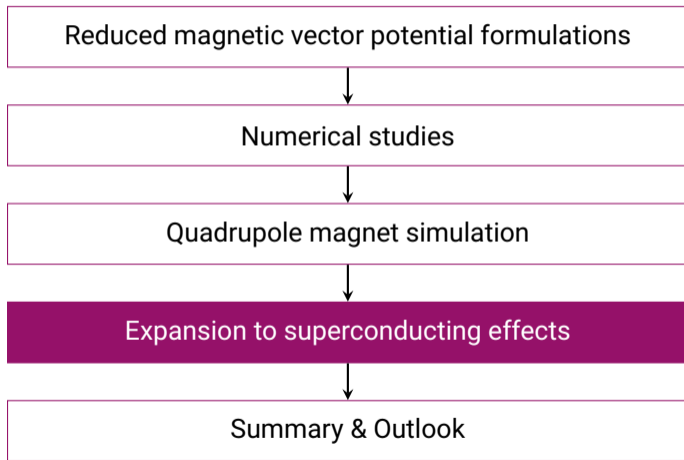


- 2D magnetostatic nonlinear simulation
- Comparison to conventional 2D FE simulation
- One line current per winding
- 488 line currents in total

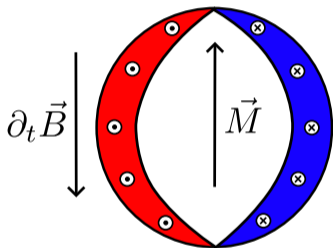
QUADRUPOLE MAGNET: SIMULATION



OUTLINE



PERFECT DIAMAGNETISM OF SUPERCONDUCTORS



Time-varying external magnetic flux density \vec{B}

↓ induces ↓

screening currents

↓ generate ↓

counter-acting magnetization \vec{M}

- This magnetization effect has to be considered in the RMVP formulation.
- **Note:** The screening current distribution in the wire gives rise to a dipole field.

HIGHER-ORDER MAGNETIC MOMENTS

Biot-Savart:

$$\vec{A}_s(\vec{r}) = \frac{\mu_0}{4\pi} \int_{V'} \frac{\vec{J}(\vec{r}')}{|\vec{r} - \vec{r}'|} dV'$$

Multipole expansion:

$$\frac{1}{|\vec{r} - \vec{r}'|} = \sum_{n=0}^{\infty} \frac{1}{n!} (-\vec{r}' \cdot \nabla)^n \frac{1}{|\vec{r}|}$$

HIGHER-ORDER MAGNETIC MOMENTS

Biot-Savart:

$$\vec{A}_s(\vec{r}) = \frac{\mu_0}{4\pi} \int_{V'} \frac{\vec{J}(\vec{r}')}{|\vec{r} - \vec{r}'|} dV'$$

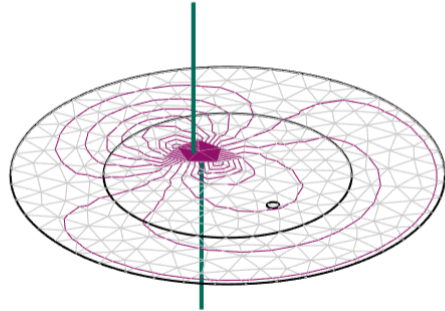
Multipole expansion:

$$\frac{1}{|\vec{r} - \vec{r}'|} = \sum_{n=0}^{\infty} \frac{1}{n!} (-\vec{r}' \cdot \nabla)^n \frac{1}{|\vec{r}|}$$

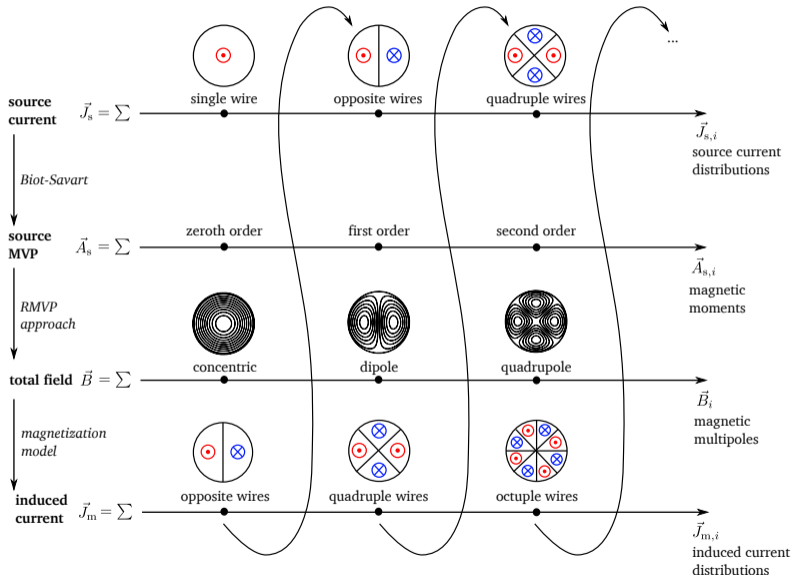
$n = 1$ (dipole):

$$\vec{A}_{s,1}(\vec{r}) = -\frac{\mu_0}{4\pi} \int_{V'} \vec{J}(\vec{r}') \frac{\vec{r} \cdot \vec{r}'}{|\vec{r}|^3} dV'$$

↔ field generated by a dipole moment at \vec{r}'
or two opposite wires around \vec{r}'



HIGHER-ORDER MAGNETIC MOMENTS



SUMMARY & OUTLOOK

Summary:

- RMVP ansatz: No explicit meshing of wires in the FE mesh
- Update: Evaluate Biot-Savart's law only on V_a at most
- High efficiency gain compared to original RMVP approach
- Consider screening currents by a dipole moment



↪ QR code to paper

SUMMARY & OUTLOOK

Summary:

- RMVP ansatz: No explicit meshing of wires in the FE mesh
- Update: Evaluate Biot-Savart's law only on V_a at most
- High efficiency gain compared to original RMVP approach
- Consider screening currents by a dipole moment

Outlook:

- Implement higher-order magnetic moments to consider magnetization and eddy current effects
- Adapt RMVP approach for high-temperature superconducting coils (tapes!)



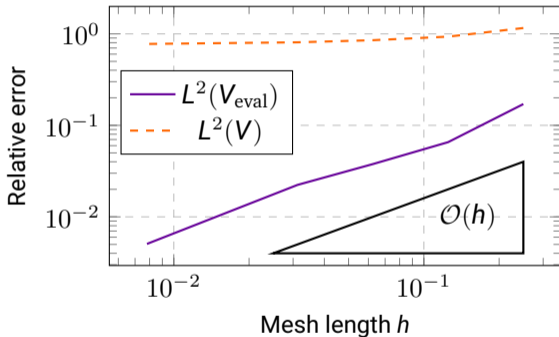
↪ QR code to paper



BACKUP SLIDES

RACETRACK COIL: CONVERGENCE STUDY

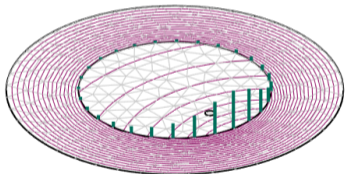
- L^2 -error w.r.t. reference solution
- Choose V_{eval} s.t. $\mathcal{L}' \not\subseteq V_{\text{eval}}$
- **Expectation** for lowest-order FEs:
Quadratic convergence of L^2 -error
(\rightarrow Aubin-Nitsche lemma)
- **Observation:** Linear convergence



DIRAC SOURCE TERM AS PROBLEM?

3. Find the reaction MVP $\vec{A}_g \in H_0(\text{curl}; V)$ s.t.

$$\left(\nu \nabla \times \vec{A}_g, \nabla \times \vec{A}'_g \right)_V = \left(\vec{n} \times \vec{H}_s, \vec{A}'_g \right)_\Gamma + \left(\vec{n} \times \vec{H}_m, \vec{A}'_g \right)_\Gamma \quad \forall \vec{A}'_g \in H_0(\text{curl}; V).$$



reaction MVP \vec{A}_g in V ,
 surface current density
 $\vec{K}_g = \vec{n} \times (\vec{H}_s + \vec{H}_m)$ on Γ

- **Hypothesis:** $\vec{J}_g = \vec{K}_g \delta_\Gamma$ as Dirac source term makes problem **not regular**
- **Literature:** **Linear convergence** of the L^2 -error of 2D elliptic problems with Dirac source term (Scott 1973)
 - Even $\mathcal{O}(h^{1/2})$ in 3D ← to check!